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Displacement-dependent microstructural and petrophysical properties of deformation bands and gouges in poorly lithified sandstone deformed at shallow burial depth (Crotone Basin, Italy)

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1 **Displacement-dependent microstructural and petrophysical properties**  
2 **of deformation bands and gouges in poorly lithified sandstone**  
3 **deformed at shallow burial depth (Crotone Basin, Italy)**

4  
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10  
11 **Keywords**

12 Cataclastic deformation bands; sub-seismic deformation features; petrophysical  
13 properties; particulate flow-cataclasis; shallow-burial depth; high-porosity sandstone.

14 **Highlights**

- 15 - Fault zone characterized by sub-seismic scale deformation features.
- 16 - Permeability drops up to 3-4 orders of magnitude with respect to pristine sandstone.
- 17 - Particulate flow operates until porosity is > 5-6%, while below cataclasis settles.
- 18 - Deformation mechanism depends upon mineralogy of grains.
- 19 - Permeability and microstructures are strictly related to the total displacement.

20 **Supplementary material**

21 Detailed description of standard operating procedures adopted during grain size analysis  
22 and all the grain size distribution curves are provided with detailed permeability, grain size  
23 data and sampling sites along the studied fault zone. Moreover, inside the online

24 supplementary file additional SEM photomicrographs, porosity, permeability data and grain  
25 shape analysis are provided with related statistical tests.

26

## 27 **ABSTRACT**

28 We present the results of meso- and micro-structural analyses performed on fault-related  
29 soft-sediment deformation structures affecting poorly lithified, high-porosity siliciclastic  
30 sediments in the Crotona Basin, Southern Italy. The investigated extensional fault zone  
31 has a total displacement of ~ 90 m and juxtaposes marine clayish sediments in the  
32 hanging wall against arkosic to lithic arkosic sandstone in the footwall. In the footwall  
33 damage zone, deformation is achieved by a network of conjugate deformation bands,  
34 whereas the foliated fault core hosts cm-thick gouges. Deformation bands and black  
35 gouges accommodated displacement between 0.2 to 20 cm. Microstructural observations  
36 and quantitative image analysis pointed out that particulate flow operated during the early  
37 stages of faulting, followed by cataclasis after significant porosity loss. Mineralogy of clasts  
38 controlled grain-scale deformation mechanism: following this, feldspar experienced  
39 extensive intragranular crushing, while quartz grains were deformed mainly by splitting and  
40 abrasion. Permeability of pristine sandstone spans from  $5.4 \times 10^4$  to  $1.4 \times 10^5$  mD, while  
41 inside deformation bands is reduced by 1-2 orders of magnitude, reaching 3-4 orders of  
42 magnitude within fault gouges. Permeability drop inside the fault zone is related to the  
43 accommodated displacement along each deformation structure, potentially leading to  
44 hydraulic compartmentalization of high-porosity sandstone reservoir.

45

## 46 **1. Introduction**

47 Fault zones in poorly lithified sediments and high-porosity rocks typically behave as  
48 barriers toward subsurface fluid flow, due to the development of deformation structures  
49 such as deformation bands and gouge layers in damage zones and fault cores,  
50 respectively (Antonellini and Aydin, 1994; Balsamo and Storti, 2010; Bense et al., 2013;  
51 Rotevatn et al., 2013; Ballas et al., 2015). Deformation bands can develop both as single  
52 structures or as clusters formed by tens to hundreds discrete elements, within which slip  
53 localizes along few discrete surfaces during progressive strain-hardening (Aydin and  
54 Johnson, 1978; Mair et al., 2000; Soliva et al., 2016; Fossen et al., 2017; Philit et al.,  
55 2018). Although strain-hardening is usually invoked as the main process leading to  
56 deformation band development, recent studies have pointed out that strain-softening may  
57 occur as well especially after reaching the yield point of the deformed material (Nicol et al.,  
58 2013). Deformation bands often show a limited lateral continuity with maximum length  
59 typically below 100 m, which is proportional to the accommodated displacement along  
60 each structure (Schultz and Fossen, 2002; Schultz et al., 2008). Fault gouges are usually  
61 found in high-strain domains and result by extreme grain size reduction and strain-  
62 localization processes (Engelder, 1974; Sibson, 1977; Balsamo and Storti, 2010).  
63 According to the classification of Sibson, (1977) the term gouge is used to identify  
64 incohesive fault rocks with less than 30% of visible clasts with respect to the fine-grained  
65 matrix. In the present contribution, we are referring to more specific fault rock types,  
66 namely black gouges, which are discrete elements showing extreme comminution and  
67 occur as isolated, or as an intricate network of deforming structures. Black gouges  
68 developing inside high-porosity sandstones were associated to a combination of grain size  
69 reduction and frictional heating produced during coseismic slip events related to shallow-  
70 depth (< 1 Km) earthquakes (Balsamo and Storti, 2011; Balsamo et al., 2014).

71 Petrophysical properties of deformation bands and fault gouges depend on several factors  
72 including lithological composition of host rock (Wilson et al., 2003; Exner and Grasemann,

73 2010; Cilona et al., 2012; Kristensen et al., 2013; Antonellini et al., 2014; Griffiths et al.,  
74 2016; Tavani et al., 2016; Cavailhes and Rotevatn, 2018), deformation mechanisms  
75 (Aydin, 1978; Aydin and Johnson, 1983; Bense et al., 2003; Rawling and Goodwin, 2003;  
76 Fossen et al., 2017), stress-strain conditions (Friedman and Logan, 1973; Olsson, 2000;  
77 Baud et al., 2012; Ballas et al., 2013; Robert et al., 2018) and microstructural features  
78 (Antonellini and Aydin, 1994; Main et al., 2000; Taylor and Pollard, 2000; Balsamo and  
79 Storti, 2011). In particular, different deformation mechanisms (cataclasis and granular-  
80 particulate flow) may cause a significant variability of permeability drops, from 1 up to 6  
81 orders of magnitude with respect to the undeformed high-porosity protoliths (Ogilvie and  
82 Glover, 2001; Balsamo and Storti, 2010; Ballas et al., 2015; Fossen et al., 2017).  
83 Permeability diminishing in siliciclastic rocks is typically achieved through processes  
84 involving grain size reduction, sorting decrease and pore space collapse (Main et al.,  
85 2000; Balsamo and Storti, 2010; Kaproth et al., 2010). The recognition of fault structure  
86 and related deformation mechanisms is critical to assess the hydrological role of fault  
87 zones in sediments or high-porosity rocks hosting aquifers or hydrocarbon reservoirs  
88 (Bense et al., 2003; Parnell et al., 2004; Sternlof et al., 2006; Fossen and Bale, 2007;  
89 Kolyukhin et al., 2010). Further, burial depth during deformation is a key parameter that  
90 may influence the permeability drop associated with deformation band development  
91 (Ballas et al., 2015).

92 Despite the significant amount of work that has been done on the genesis and evolution of  
93 deformation bands (e.g., Antonellini et al., 1994; Cashman and Cashman, 2000; Mair et  
94 al., 2002a; Balsamo and Storti, 2010; Kaproth et al., 2010; Charalampidou et al., 2011;  
95 Fossen et al., 2017), basic scaling-laws such as the relationships between displacement  
96 and petrophysical properties are still a matter of debate (Torabi and Fossen, 2009; Ballas  
97 et al., 2012; Rotevatn et al., 2013, 2017). Previous studies mainly focused on the  
98 permeability ratio between faulted and undeformed rocks (Ballas et al., 2015; Fossen et

99 al., 2017). With the present contribution, we attempt to provide additional details  
100 concerning the effect of total accommodated displacement on the microstructural features  
101 of deformation bands and gouges formed at shallow-burial conditions. Furthermore, the  
102 influence of microstructural-textural and petrophysical properties upon overall permeability  
103 was analyzed. For this purpose, we investigated in detail the microstructural and  
104 petrophysical properties of sub-seismic scale deformation structures occurring along the  
105 Rocca di Neto extensional fault zone affecting Pleistocene high-porosity sandstones in the  
106 Croton Basin, Southern Italy. The footwall damage zone of the Rocca di Neto fault zone  
107 is characterized by widespread occurrence of deformation bands, both as single elements  
108 as well as clusters, and subsidiary faults with different amounts of displacement and grain  
109 size comminution. Black gouge layers are abundant in the foliated fault core, adjacent to  
110 the master slip zone. In this study, such sub-seismic scale structural elements were  
111 studied both at the meso and at the micro-scale. Petrophysical properties of deformed and  
112 undeformed sediments (permeability, grain size and porosity) were measured both by *in*  
113 *situ* and laboratory analyses. Complementary image analysis was used to quantify the  
114 grain shape and their preferred orientation. This multidisciplinary approach allowed us to  
115 constrain the evolution of deformation mechanism during faulting, which progressed from  
116 particulate flow to cataclasis, and to quantify the role of displacement in determining the  
117 petrophysical properties of faulted sandstones.

118

## 119 **2. Geological setting and fault zone structure**

120 The study area is located in the Croton forearc basin, in Southern Italy (Fig. 1a), which  
121 developed as a consequence of subduction of the Adria plate below the European plate  
122 (e.g., Van Dijk et al., 2000; Zecchin et al., 2004; Reitz and Seeber, 2012). Basin infill  
123 began in Middle Miocene times, resulting in a stratigraphic succession as thick as 2500 m,

124 overlying the metamorphic basement of the Sila Massif (Zecchin et al., 2004, 2012). Basin  
125 evolution includes five subsidence-uplift events during a dominant extensional and subtle  
126 transpressional tectonic history (Van Dijk and Scheepers, 1995; Van Dijk et al., 2000;  
127 Ferranti et al., 2009). Eventually, the onset of regional uplift since Middle Pleistocene  
128 times, led to the cessation of sedimentation and at the same time to the exhumation and  
129 surface exposure of the sedimentary succession (Knott and Turco, 1991; Antonioli et al.,  
130 2006; Zecchin et al., 2012; Massari and Prosser, 2013).

131 The present-day tectonic architecture of the onshore portion of the basin is defined by two  
132 major left-lateral shear zones bounding the basin to the NE and to the SW. A set of NE-  
133 SW-striking extensional fault zones accommodates displacement of several tens to  
134 hundreds meters in the centre of the basin (Van Dijk, 1994; Zecchin et al., 2004) (Fig. 1b).  
135 The Rocca di Neto fault zone belongs to the latter extensional fault system and affects  
136 Pleistocene sediments pertaining to the late-stage basin infill (Fig. 1c). In particular, the  
137 fault zone juxtaposes clayish sediments (Cutro Clay) in the hanging wall against silty  
138 sands, sandstones and conglomerates (Scandale Sandstone) in the footwall block  
139 (Zecchin et al., 2012) (Figs. 1c and 2a). The Cutro Clay was deposited in an offshore,  
140 shallow-marine environment, while the deposition of the Scandale Sandstone occurred in  
141 a shoreface setting where the majority of sediment supply was provided by a nearby river  
142 delta (Zecchin et al., 2012). Due to the unconsolidated nature of faulted sediments, the  
143 fault zone displays extensive occurrence of deformation features affecting high-porosity  
144 rocks (Balsamo and Storti, 2010; Pizzati et al., 2019), namely deformation bands and fault  
145 gouges. These structures are exclusively present in the footwall block of the fault, where  
146 high-porosity sandstones crop out. Conversely, the hanging wall block is almost  
147 completely covered by vegetation due to the presence of clayish sediments (Fig. 2a).  
148 Deformation bands are thin and well-localized tabular features that, when arranged in  
149 conjugate sets, typically have displacement between 1 and 5 cm. Deformation bands with

150 displacement < 1 cm are found far from subsidiary faults and deformation band clusters.

151 Fault-parallel deformation bands located closer to the master fault can display higher

152 offsets, from 5 to 10 cm. Subsidiary faults accommodate larger amounts of displacement

153 (> 15-20 cm) and are characterized by several cm-thick slip surfaces.

154 The overall structural architecture of the exposed footwall of the Rocca di Neto fault zone

155 consists of four structural domains (Pizzati et al., 2019) (Fig. 2a, b): (1) a low-deformation

156 zone, with widely spaced deformation bands and few subsidiary faults having low-

157 displacement (Fig. 2b, c); (2) the damage zone, characterized by abundant conjugate

158 deformation bands, together with subsidiary faults showing antithetic and synthetic shear

159 sense with respect to the master fault (Fig. 2b, c); (3) the mixed zone, with a dense

160 network of conjugate and high-strain fault-parallel deformation bands (Fig. 2b, c); (4) the

161 fault core formed by foliated coarse to very fine sand cut by slip surfaces decorated by

162 mm-to cm-thick black gouges (Fig. 2b, c). Although the majority of the total displacement is

163 accommodated along the mixed zone and fault core, deformation bands and gouges

164 significantly contribute to the offset partitioning along the entire fault zone.

165 Inside the low-deformation zone, and to lesser extent in the outer part of the footwall

166 damage zone, deformation bands are arranged in conjugate sets and have offsets typically

167 lower than ~ 1 cm (Fig. 3a). In the footwall damage zone, deformation bands are arranged

168 in three sets; two of them form an inclined conjugate system (hereafter DB<sub>1</sub> and DB<sub>2</sub>),

169 while the third one (DB<sub>3</sub>) is parallel to subsidiary faults (Fig. 3b). Within the mixed zone,

170 deformation bands are organized in dense arrays, mostly trending parallel to subsidiary

171 synthetic faults and to lesser extent arranged in conjugate arrays similar to the adjacent

172 damage zone (Fig. 3c). Several 5-20 cm-thick clusters of fault-parallel deformation bands

173 developed both in the damage zone and mixed zone, have cumulative offset typically

174 exceeding 10 cm.



175 The studied cross-sectional exposure includes also the fault core, where most of the  
176 displacement is accommodated. This structural domain hosts several anastomosing slip  
177 surfaces decorated by black gouges (Fig. 2a, c) with thickness of ~ 1 cm, locally  
178 developing a gently folded pattern (Fig. 3d). Foliated sand encasing black gouges is highly  
179 deformed and tectonically compacted (Pizzati et al., 2019).

180 Inside the fault zone deformation bands and subsidiary faults often display evidence for  
181 selective cementation in the form of carbonate concretions made of calcite. Carbonate  
182 concretions develop tabular-to lens-shaped cemented bodies with thickness ranging from  
183 a few cm to 10-20 cm, paralleling the surface of the structural elements they encase (Fig.  
184 3c, d). Cementation affects only deformation bands and subsidiary faults, while the host  
185 sandstone is completely non-cemented, except for rare, thin, bedding-parallel concretions  
186 displaying limited lateral continuity.

187

### 188 **3. Analytical methods**

#### 189 *3.1. Grain size analysis by laser diffraction*

190 Sediment grain size was measured on 68 samples collected from different positions  
191 throughout the fault zone, according to the sediment type, position with respect to the  
192 master fault, and displacement (sampling sites are reported in Fig. 2a and Fig. A3 in the  
193 Supplementary Material). Samples were first dried at a constant temperature of 45°C for  
194 48 hours, and then sieved with a 2000 µm mesh to remove impurities. Grain size analysis  
195 was performed with a Mastersizer 3000 (Malvern Instruments) laser diffraction particle size  
196 analyzer having an operating size range spanning from 0.01 to 3500 µm. In particular, we  
197 used the Hydro EV wet dispersion unit, with distilled water as dispersant fluid. Different  
198 analytical procedures were specifically developed for each sample type in order to  
199 minimize the alteration during the analysis (e.g. Storti and Balsamo, 2010). Details of tests

200 and final grain size distributions are provided in the online Supplementary Material. Based  
201 on the grain size distribution curves, mean grain size, mode, span (sorting), and fractal  
202 dimension (D-value) were calculated. Span is defined as the width of the grain size  
203 distribution, while the D-value is calculated as the slope of the best-fit power-law  
204 distribution between grain size and cumulative frequency of particles per each grain size  
205 class in a log-log graph (Blenkinsop, 1991; Rawling and Goodwin, 2003; Balsamo and  
206 Storti, 2011).

### 207 *3.2. In situ air permeability*

208 A total of 652 *in situ* permeability measurements were performed across the fault zone  
209 using a portable Tiny Perm II air-permeameter (New England Research), which provides  
210 accurate data between  $10^{-1}$  and  $10^5$  mD, according to the methodology described by  
211 Balsamo et al. (2013). Permeability measurements were performed in the same sites  
212 where grain size samples were collected (see Fig. 2a and Figs. A2 and A3 in the online  
213 Supplementary Material), after careful brushing the target sediment to remove any  
214 alteration crust.

### 215 *3.3. Image analysis technique*

216 Fifty-five polished thin sections impregnated with blue-dyed resin were scanned at high  
217 resolution with a Nikon SuperCoolScan 5000 and studied with a Zeiss Axioplan 2  
218 petrography microscope and a JEOL JSM 6400 scanning electron microscope (SEM),  
219 operating at 240 nA and 20 kV beam current. Two-dimensional porosity calculations were  
220 performed on 273 selected images acquired with the petrographic microscope at 12.5×  
221 magnification (thin section area 4747×3560  $\mu\text{m}$ ), both for the undeformed and faulted  
222 sandstone, using ImageJ open-source image analysis software (Schneider et al., 2012). A  
223 multi-scale image analysis technique was used to quantitatively describe particle shape. In

224 particular, grains with equivalent diameter between 95 and 500  $\mu\text{m}$  were investigated with  
225 12.5 $\times$  magnification, from 35 to 95  $\mu\text{m}$  with 25 $\times$  magnification (2352 $\times$ 1764  $\mu\text{m}$ ), from 25 to  
226 35  $\mu\text{m}$  with 50 $\times$  magnification (1242 $\times$ 932  $\mu\text{m}$ ) and those between 10 and 25  $\mu\text{m}$  with 100 $\times$   
227 magnification (614 $\times$ 461  $\mu\text{m}$ ). Particles finer than 10  $\mu\text{m}$  were not taken into account  
228 because of their size below the resolution limit of the 100 $\times$  optical microscope  
229 magnification. Particles with equivalent diameter greater than 500  $\mu\text{m}$  are rare due to the  
230 medium-fine grain size of the analyzed samples. Grains were manually digitized at each  
231 magnification to prevent any bias and inaccuracy induced by the auto-tracing methods.  
232 Particle shape data were plotted against five grain size classes from 0 to 250  $\mu\text{m}$ , with 50  
233  $\mu\text{m}$  bin size. Typically, more than 30 data were collected and averaged for each grain size  
234 class to grant statistical significance of the shape descriptors.  
235 Three shape descriptors were used, namely aspect ratio, circularity and solidity. Aspect  
236 ratio (AR) is defined as:

$$237 \quad AR = \frac{\text{Major axis}}{\text{Minor axis}} \quad (1)$$

238 where *Major axis* indicates the segment connecting the two farthest points along the  
239 perimeter of the grain, while *Minor axis* is the segment having as tips the nearest points on  
240 the perimeter. Values span from 1 (equant particle) to infinity (very elongated particle).

241 Circularity (C) is given by:

$$242 \quad C = \frac{4\pi A}{p^2} \quad (2)$$

243 where  $A$  is the total area of the grain and  $p$  is the perimeter. Circularity spans from 0  
244 (extremely elongated and irregular shape) to 1 (perfect circle). Solidity (S) is defined as:

$$245 \quad S = \frac{A}{A_{conv}} \quad (3)$$

246 where  $A_{conv}$  is the convex area delimited by the convex hull. Solidity varies from 0 (grain  
247 with extremely rough surface) to 1 (grain with very smooth surface).

248 Grain preferred orientation was also analyzed by measuring the angle between grain  
249 major axis and a horizontal reference plane. Half-rose diagrams were produced, using  
250 dotted lines to represent orientations of the investigated deformation structures in the thin  
251 sections.

252

## 253 **4. Petrographic and microstructural characterization**

### 254 *4.1. Petrography of undeformed sandstone*

255 The composition of the undeformed sandstone was constrained by modal analysis on 35  
256 selected photomicrographs acquired at 12.5× magnification (thin section area 4747×3560  
257 μm), via image analysis extracting the area percentage of the most recurrent mineralogical  
258 species. According to the results, 23 pristine sandstone samples lay in the lithic arkose  
259 field, while 12 of them plot in the arkose field in the Q-F-L ternary diagram of Folk (1974)  
260 (Fig. 4a). In particular, quartz percentage spans from 50.3 to 67.7%, while feldspar ranges  
261 from 19.6 to 36.9% and lithics from 5.3 to 18.2%. Lithics mainly include gneiss and granitic  
262 rock fragments, but sedimentary detrital grains also occur in the form of calcite grains and  
263 fossil shells. Other less frequent lithics are biotite mica, iron oxides-hydroxides, rare  
264 muscovite, chlorite and glauconite.

### 265 *4.2. Microstructures*

266 Deformed sandstone shows a variety of microstructures, according to the total  
267 displacement. In the low-deformation zone, deformation bands are tabular structures with  
268 a minimum thickness of 1-5 mm and sharp boundaries with the surrounding pristine  
269 sandstone (Fig. 4b). Grain size reduction is negligible and depositional fabric re-

270 organization results in significant porosity loss. Deformation bands having few cm of  
271 displacement show grain size reduction, mainly produced by fragmentation of coarser  
272 feldspar grains and quartz abrasion (Fig. 4c). In particular, feldspar grains are deformed by  
273 several intragranular fractures, leading to the formation of tens of clasts, while quartz  
274 grains show mostly splitting and flaking of asperities (Fig. 5a, b). When displacement  
275 approaches or overcomes 10 cm, deformation bands are up to 5-6 mm-thick and display  
276 outer sectors made of comminute and crushed grains, and ~ 300  $\mu\text{m}$ -thick cores where  
277 grain size reduction is more intense (Fig. 4d). The abundant dark brown matrix is  
278 dominantly composed of crushed feldspar and lithic grains, together with fine-grained  
279 quartz chips and to lesser extent fragments of detrital calcite. Locally, feldspar and quartz  
280 oversized survivor grains are present within the core of deformation bands and are  
281 cushioned by finer particles, which prevented their fracturing (Fig. 5c, d).

282 Black gouges have complex microstructural features, characterized by the presence of  
283 ultra-comminute 500-1000  $\mu\text{m}$ -thick slip zones encased by less comminute sand volumes  
284 where subtle S-C structures are imparted by preferential orientation of mica flakes and  
285 coarse survivor grains (Fig. 4e). Fault cores of subsidiary faults show intense grain size  
286 comminution with several oversized survivor grains surrounded by a fine-grained matrix  
287 (Fig. 4f). Along deformation bands and gouges grain fracturing markedly occurs in their  
288 outer portion, whereas in the interior clasts are rarely affected by fractures (Fig. 6a). A  
289 gradient of comminution intensity is frequently observed in deformation band cores,  
290 resulting in the progressive increase of grain size from one boundary to the other (in Fig.  
291 6b the left (footwall side) boundary of the deformation band is more comminute than the  
292 right side). High-displacement deformation bands sampled in the footwall damage zone  
293 commonly display a more pronounced grain size reduction on the footwall side.  
294 Conversely, deformation bands inside the fault core and mixed zone are characterized by  
295 asymmetric grain size reduction on the hanging wall side. Black gouges show the same

296 gradient of grain size reduction as the one observed in deformation bands, but typically it  
297 is more intense along the hanging wall rather than on the footwall side (right side in Fig.  
298 6c); thus these deformation elements display an asymmetric structure at the micro-scale.

299

## 300 **5. Grain size data**

301 Undeformed protoliths in the low-deformation zone are mainly composed of well-sorted,  
302 medium-to fine-grained sand with a mean size of 334  $\mu\text{m}$  and, subordinately, medium-  
303 coarse sand with a mean size of 501  $\mu\text{m}$  (Fig. 7a and table 1). Span values are very low  
304 for both sediment types (1.7 and 1.2, respectively; Fig. 7b). In the low-displacement zone,  
305 deformation bands have mean grain size of 236  $\mu\text{m}$ , a mean span of 3.3 (Fig. 7a, b).

306 Moving to the footwall damage zone, the mean grain size of medium-fine sand layers  
307 composing the interband domain (i.e., the sand volume in between two adjacent  
308 deformation bands) decreases to 249  $\mu\text{m}$ , whereas interband coarse sand has mean grain  
309 size of 614  $\mu\text{m}$  (Fig. 7a), with mean span values of 1.9 and 3.1, respectively (Fig. 7b).

310 Conjugate deformation bands with different displacement magnitude inside the footwall  
311 damage zone display a range of grain size from 127 to 339  $\mu\text{m}$ , while span varies from 4.6  
312 to 8.1 (Fig. 7a, b).

313 Subsidiary faults and thick clusters of deformation bands have a mean grain size of 123  
314  $\mu\text{m}$  and a mean span of 5.8 (Fig. 7a, b).

315 Inside the footwall mixed zone, foliated sand is characterized by a mean grain size of 54  
316  $\mu\text{m}$  and a mean span of 9.2. Along the same structural domain, thin black gouges display  
317 mean grain size of 57  $\mu\text{m}$ , with a mean span of 12.8 (Fig. 7a, b).

318 The fault core hosts foliated and stretched coarse sand pods characterized by a mean  
319 grain size of 428  $\mu\text{m}$  and mean span of 4.3 (table 1). Foliated very fine sand displays a  
320 mean grain size of 84  $\mu\text{m}$ , with mean span of 5.4. Eventually, black gouges in the fault

321 core are characterized by mean grain size of 49  $\mu\text{m}$  and a mean span of 11.2 (Fig. 7a, b).  
322 Details on granulometric curves of undeformed and deformed sediment samples are  
323 provided in the online Supplementary Material and in table 1.

324 Overall, low-displacement deformation bands induce an almost 2 times decrease of mean  
325 grain size, while medium-to high-displacement bands may reach mean grain size 3 times  
326 finer than the undeformed medium-fine sand. Black gouges and foliated very fine sand  
327 inside the fault core are characterized by mean grain size 7 and 5 times finer than the  
328 corresponding pristine medium-fine sand, respectively. Deformed sediment samples show  
329 a progressive increase in span, with the highest values characterizing deformation  
330 features inside the mixed zone and fault core (Fig. 7a, b).

331 While the comparison of samples in Figure 7 provides a summary of grain size data  
332 through the entire fault zone, accurate analysis of grain size variability induced by  
333 deformation is possible by evaluating granulometric curves of adjacent sample pairs as in  
334 Figure 8 (Storti et al., 2003). To this end, representative samples of deformation bands  
335 and gouges characterized by different displacement magnitudes were compared with the  
336 adjacent host sediments (undeformed in the low-deformation domain, and tectonically  
337 compacted foliated sand within mixed zone and fault core). In particular, a low-  
338 displacement deformation band collected inside the low-deformation zone is characterized  
339 by a mean grain size of 185  $\mu\text{m}$  with a modal peak at 225  $\mu\text{m}$ , while the undeformed  
340 medium-fine sand has a mean grain size of 280  $\mu\text{m}$  and a modal peak at 320  $\mu\text{m}$  (Fig. 8a).  
341 The shape and span of the grain size distribution curves are almost the same. Although  
342 similar, the D-value of the deformation band is slightly higher compared to the undeformed  
343 host sand (2.307 and 2.242, respectively) (Fig. 8b). The ratio between the number of  
344 faulted vs undeformed particles points out a relative increase of particles between the  
345 range from 0.4 to 240  $\mu\text{m}$  in the deformation band and a decrease of coarse particles from  
346 240 to 500  $\mu\text{m}$  (Fig. 8c). The medium-displacement deformation band collected inside the

347 footwall damage zone is characterized by a mean grain size of 155  $\mu\text{m}$ , having a modal  
348 value of 225  $\mu\text{m}$ , whereas the undeformed counterpart has a mean grain size of 248  $\mu\text{m}$   
349 with modal value of 200  $\mu\text{m}$  (Fig. 8d). The D-value shows marked differences between the  
350 two samples, with the medium-displacement deformation band attesting at 2.634, while the  
351 adjacent interband domain has 2.3 (Fig. 8e). The deformed domain is characterized by an  
352 increase in fine particles in the range between 0.4 and 86  $\mu\text{m}$ , with respect to the  
353 undeformed sample, while displays a decrease of coarse particles from 86 to 1630  $\mu\text{m}$   
354 (Fig. 8f). High-displacement deformation band in the footwall damage zone has a mean  
355 grain size of 95  $\mu\text{m}$  having slightly pronounced trimodal distribution with relative maxima at  
356 0.7, 30 and 230  $\mu\text{m}$  (Fig. 8g). The interband domain is characterized by mean grain size of  
357 248  $\mu\text{m}$  with a modal value of 200  $\mu\text{m}$ . The span of the grain size distributions is different  
358 with the deformation band showing a wider curve with respect to the undeformed control  
359 sample. D-value of the high-displacement deformation band is 2.769, much higher than  
360 the one characterizing the undeformed sand in the interband domain (2.3) (Fig. 8h). Below  
361 the 65  $\mu\text{m}$  threshold, the high-displacement deformation bands shows a relative increase  
362 of particle number with respect to the undeformed host sand (Fig. 8i). Moving to the mixed  
363 zone, the fault core of a subsidiary fault displays mean grain size of 98  $\mu\text{m}$ , with a trimodal  
364 distribution having relative maxima at 0.7, 29 and 160  $\mu\text{m}$ . The adjacent sediment is  
365 formed by foliated sand with mean grain size of 72  $\mu\text{m}$ , having similar distribution to the  
366 previous sample with relative maxima at 0.7, 26 and 153  $\mu\text{m}$  (Fig. 8j). Span of the two  
367 granulometric distributions is almost the same. The fault core of the subsidiary fault has a  
368 D-value of 2.866 while for the foliated host sand is 2.776 (Fig. 8k). Inside the fault core of  
369 subsidiary fault the number of particles increases in the interval between 0.3 and 6.5  $\mu\text{m}$ ,  
370 and from 240 to 350  $\mu\text{m}$ , while it decreases from 6.5 to 240  $\mu\text{m}$  (Fig. 8l). Eventually, a  
371 black gouge sample inside the fault core is characterized by a mean grain size of 32  $\mu\text{m}$ ,  
372 with trimodal distribution having maxima at 0.6, 8 and 81  $\mu\text{m}$  (Fig. 8m). The adjacent



373 sediment is composed of foliated very fine sand with a mean grain size of 78  $\mu\text{m}$  and a  
374 bimodal distribution with relative peaks at 0.7 and 62  $\mu\text{m}$ . The D-value of black gouge is  
375 substantially higher than the one calculated for the foliated very fine sand (3.191 and  
376 2.747, respectively) (Fig. 8n). Black gouge is characterized by an increase in the number  
377 of particles from 0.5 to 14.5  $\mu\text{m}$  and from 516 to 586  $\mu\text{m}$ , and by a relative decrease from  
378 14.5 to 516  $\mu\text{m}$  with respect to the foliated host sand (Fig. 8o).

379

## 380 **6. Petrophysical properties**

### 381 *6.1. Permeability measurements*

382 Along the footwall of the fault, *in situ* air-permeability shows a progressive decrease from  
383 the low-deformation zone toward the fault core (Fig. 7c). The highest permeability is  
384 recorded by medium-to fine-grained and coarse sandstone in the low-deformation domain,  
385 with mean values of  $5.4 \times 10^4$  and  $1.4 \times 10^5$  mD, respectively (Fig. 7c). Deformation bands  
386 with displacement < 1 cm, have almost half of the permeability shown by undeformed  
387 sandstone ( $3.1 \times 10^4$  mD). In the footwall damage zone, relatively undeformed medium-  
388 fine and coarse sandstones in the interband domain are characterized by mean  
389 permeability of  $1.2 \times 10^4$  and  $5.3 \times 10^4$  mD, respectively. Permeability in these interband  
390 sandstones shows a drop of at least half order of magnitude with respect to the  
391 undeformed sediments. Conjugate DB<sub>1</sub> and DB<sub>2</sub> sets inside the footwall damage zone  
392 have permeability spanning from  $2.6 \times 10^3$  to  $7.4 \times 10^3$  mD, thus causing a drop from 1 to  
393 1.5 orders of magnitude (Fig. 7c). Fault core of subsidiary faults and thick clusters of  
394 deformation bands are characterized by a permeability drop up to 2 orders of magnitude  
395 (Fig. 7c). From the inner damage zone to the mixed zone, permeability shows an abrupt  
396 decrease in foliated sand layers and in thin black gouges (mean permeability of 193 and  
397 201 mD, respectively) (Fig. 7c). Black gouges in fault core have mean permeability of 245

398 mD, with 7 mD as the lowest recorded value, thus featuring an overall permeability drop of  
399 3 to 4 orders of magnitude with respect to the undeformed sandstone. In the same  
400 domain, foliated very fine sand and stretched very coarse sandstone recorded mean  
401 permeability of 496 and 4026 mD, respectively (Fig. 7c).

## 402 *6.2. Two-dimensional porosity calculation*

403 Primary porosity was calculated from acquired images neglecting any secondary porosity  
404 related to rare tensile micro-fractures and dissolution of fossil shells. Undeformed  
405 sandstone samples, from fine-to coarse-grained, have a mean 2-D porosity of 37.6% with  
406 a wide range of variation between 27.5 and 50.6% (Fig. 7d). Sediment volumes between  
407 deformation bands, both in the low-deformation and in the damage zone domains  
408 (interband domain), show a mean 2-D porosity of 29.7%. In the footwall damage zone,  
409 deformation bands with different displacement magnitude display a wide range of porosity  
410 values from 0.3 to 31.9% with a mean of 3.9% (Fig. 7d). Subsidiary faults and thick  
411 clusters of deformation bands inside the inner part of the damage zone are characterized  
412 by a mean porosity of 1.1%. In the footwall mixed zone, foliated sand volumes outside  
413 deformation bands have a mean porosity of 2.2%, while thin black gouges reach 1% (Fig.  
414 7d). Eventually, foliated coarse sand pods in the fault core display a mean porosity of  
415 2.9%, while foliated very fine sand reaches 0.8%. Black gouges encompassing the master  
416 fault are again characterized by very low porosity values below 1% (Fig. 7d).

417 At the micro-scale, porosity calculation performed along transects through deformation  
418 bands provides more details relative to porosity distribution (Fig. 9). In particular, a strand  
419 of low-displacement deformation bands has an almost symmetrical decrease of porosity  
420 (porosity decrement is almost the same on both sides of the deformation band) (Fig. 9a).  
421 On the contrary, a high-displacement deformation band has more pronounced asymmetry  
422 of porosity decrease from side to side (Fig. 9b). In this sample, porosity shows a more

423 gradual diminishing from left to right, while on the right side the decrease is more abrupt at  
424 the sharp contact with undeformed sand. Porosity values reflect the different grain size  
425 distribution along the deformation band due to the development of a preferential slip  
426 surface. The vast majority of deformation bands tend to localize the shear along the  
427 hanging wall side, but also a few samples with localization along the footwall side were  
428 documented. Eventually, the black gouge has a marked asymmetric porosity diminishing  
429 approaching the preferential slip surface localized on the right side of the figure (Fig. 9c).  
430 These deformation features are formed by several preferential slip zones contributing to  
431 the major internal complexity with respect to deformation bands. However, also in black  
432 gouges a major preferential slip zone can be identified and corresponds to the sharp  
433 porosity contrast between undeformed and deformed sand (Fig. 9c). Differently to  
434 deformation bands, black gouges localize strain solely along their hanging wall side.

435

## 436 **7. Grain shape data**

### 437 *7.1. Cumulative data*

438 In Figure 10 are shown the grain shape descriptors (aspect ratio, circularity and solidity)  
439 versus grain size classes for deformation bands (low, medium and high-displacement),  
440 black gouges and subsidiary faults. All grain shape data are reported as ratio between  
441 faulted and undeformed particles, so that the following graphs show the relative increase-  
442 decrease of shape parameters in comparison with the reference sandstone. The  
443 undeformed reference sample used is a medium-to fine-grained sand belonging to the low-  
444 deformation zone (detailed shape data of the undeformed reference sample are reported  
445 in the online Supplementary Material Fig. A8). Overall, the aspect ratio of grains  
446 composing the deformed domains is lower than the reference undeformed sample  
447 throughout almost the entire investigated grain size interval. Thus, deformed grains tend to

448 be more equant than undeformed ones (Fig. 10a). The lowest aspect ratio values are  
449 recorded in the grain size interval between 0 and 100  $\mu\text{m}$ , while at coarser grain size they  
450 increase approaching the undeformed reference sand. Only in the 200-250  $\mu\text{m}$  interval,  
451 two deformation band samples show aspect ratio values above the undeformed reference,  
452 featuring an increase of particle elongation. Circularity of deformed particles is higher than  
453 undeformed medium-fine sand, with only two mean values lying below the reference in the  
454 200-250  $\mu\text{m}$  range (Fig. 10b). Following this, deformed particles have more regular and  
455 circle-like shape than grains composing the undeformed control sample. The highest  
456 circularity values are recorded in the finest grain size interval (0-50  $\mu\text{m}$ ), with a progressive  
457 decrease at coarse grain size classes (Fig. 10b). Eventually, solidity of deformed domains  
458 is higher compared to the undeformed sand except for one deformation band sample in  
459 the 200-250  $\mu\text{m}$  grain size class (Fig. 10c). According to this, faulted particles display a  
460 smoother outer surface, with less asperities than the reference sample. Highest solidity  
461 values are shown in the finest grain size range (0-50  $\mu\text{m}$ ), while they progressively  
462 diminish with increasing grain size (Fig. 10c).

463 More details are provided by the comparison of grain shape data of the representative five  
464 structural deformation features taken into account. In particular, the aspect ratio values  
465 show a progressive diminishing through the entire grain size range considering low,  
466 medium, high-displacement deformation bands and the black gouge. The difference  
467 between each dataset is more pronounced at finer grain size, while values converge in  
468 coarser grain size classes (Fig. 10a). The subsidiary fault displays aspect ratio between  
469 the low and medium-displacement deformation bands. Comparison of circularity between  
470 single structures points out low-displacement deformation band having the lowest values,  
471 while black gouge has the highest ones (Fig. 10b). Medium and high-displacement bands  
472 lay in between the previously mentioned structures, with the subsidiary fault covering the  
473 low-circularity interval partially overlapping with low-to-medium-displacement bands (Fig.

474 10b). As seen before for the aspect ratio, also differences in circularity are more evident in  
475 the finer grain size classes, while they are less emphasized in the coarser range.  
476 Eventually solidity between the five structural features displays trends similar to circularity.  
477 In particular, a progressive increase of particle smoothness from low-displacement  
478 deformation band to black gouge is observed, with medium-to-high-displacement bands  
479 lying in between (Fig. 10c). The subsidiary fault sample is characterized by values  
480 overlapping with low-and medium-displacement deformation bands. Differences between  
481 each dataset are more pronounced in the fine grain size range rather than in the coarse  
482 one (Fig. 10c). In summary, (i) aspect ratio of deformed particles is generally lower (more  
483 equant shape) than the undeformed sample; (ii) circularity of faulted grains is higher (more  
484 rounded shape) than undeformed ones; (iii) solidity is higher (smoother grains) in faulted  
485 domains; (iv) the difference of shape descriptors from deformed to undeformed domains is  
486 more evident with increasing displacement, except for the subsidiary fault, which seems  
487 not to follow this trend.

488 For statistical analysis of the entire grain shape dataset the reader is referred to the on-line  
489 Supplementary Material tables A2, A3 and A4.

## 490 *7.2. Quartz, Feldspar, and Lithic grain shape data*

491 Figure 11 displays the shape descriptors (aspect ratio, circularity and solidity) versus grain  
492 size classes for deformation bands (low, medium and high-displacement), black gouges  
493 and subsidiary faults, subdivided according to grain mineralogy (quartz, feldspar and lithic  
494 fragments). All grain shape data are reported as ratio between faulted and undeformed  
495 particles; the undeformed reference sample is the same medium-to fine-grained sand used  
496 in Figure 10 (detailed shape data of the undeformed reference are reported in the online  
497 Supplementary Material Fig. A10). As a general observation, aspect ratio of the three  
498 dominant mineralogical phases is below the undeformed sandstone adopted as reference.

499 Thus, quartz, feldspar and lithic deformed grains are more equant than the undeformed  
500 ones (Fig. 11a). Quartz grains have higher aspect ratio values than feldspar and lithics  
501 especially in the finer (0-100  $\mu\text{m}$ ) and coarser (150-200  $\mu\text{m}$ ) grain size ranges, while the  
502 difference is less evident from 100 to 150  $\mu\text{m}$  (Fig. 11a). The circularity graph shows that  
503 almost all plotted mean data are above the reference sample except for the quartz data  
504 belonging to subsidiary fault in the 150-200  $\mu\text{m}$  range. This suggests that all three  
505 mineralogical species are characterized by higher circularity values than the undeformed  
506 sand (Fig. 11b). Quartz has lower values compared to feldspar and lithics throughout the  
507 entire grain size range. Conversely, feldspar has the highest value in the 0-50  $\mu\text{m}$  grain  
508 size class, while at coarser grain size is exceeded by lithic fragments (Fig. 11b). Solidity  
509 graph indicates an increase of grain smoothness for quartz, feldspar and lithics in the  
510 entire investigated grain size interval, except for the quartz data characterizing the  
511 subsidiary fault in the 150-200  $\mu\text{m}$  interval (Fig. 11c). Similarly to trends identified for  
512 circularity, also solidity shows quartz having lower mean values compared to feldspar and  
513 lithics. Through the observation of trends from every deformation structures it stems that  
514 the decrease of aspect ratio for quartz, feldspar and lithics with respect to undeformed  
515 sand is more pronounced at finer grain size. Conversely, in the coarse size range aspect  
516 ratio diminishing is less marked (Fig. 11a). Increasing offset from low-displacement band  
517 to black gouge is reflected by an overall wider aspect ratio difference with the undeformed  
518 control sample and by a more evident difference between quartz, feldspar and lithics in the  
519 fine-grained interval. Despite having the highest displacement, the subsidiary fault has  
520 aspect ratio values similar to the low-displacement deformation band (Fig. 11a). Also for  
521 circularity the increase of displacement is reflected in a wider difference between  
522 undeformed and deformed domains and also between quartz, feldspar and lithics along  
523 the same deformation structure. This difference is particularly marked in the finer grain  
524 size classes (0-100  $\mu\text{m}$ ), while it becomes faint and less easily distinguishable in the

525 coarser interval (Fig. 11b). As pointed out before for the aspect ratio, also circularity of  
526 subsidiary fault has values comparable to deformation bands with limited offset. Solidity  
527 suggests trends between the three mineralogical species very similar to what described for  
528 circularity, with a marked difference with respect to the undeformed sample in the fine  
529 grain size classes (0-100  $\mu\text{m}$ ) and less pronounced in coarse interval (100-200  $\mu\text{m}$ ) (Fig.  
530 11c). Also in this case, the subsidiary fault shows relatively low solidity values comparable  
531 to low-displacement deformation bands.

532 To summarize, (i) quartz grains are generally the more elongated and angular particles; (ii)  
533 feldspar grains are less elongated and more rounded than quartz; (iii) lithic fragments have  
534 highly varying shape descriptors; (iv) grain shape differences between quartz, feldspar and  
535 lithics generally increase with increasing displacement of deformation structures and are  
536 more marked at finer grain size range. The statistical analysis of grain shape dataset is  
537 provided in tables A4-A13 in the online Supplementary Material.

538

## 539 **8. Grain preferential orientation**

540 Grain preferential orientation was performed by calculating the angle between grain major  
541 axis and a reference horizontal plane. Data presented are not differentiated according to  
542 the mineralogy of grains (quartz, feldspar and lithics), so that they report the bulk  
543 preferential orientation of deformed and undeformed sand.

544 Low-displacement deformation band displays a weak grain preferential alignment parallel  
545 to the band direction, as highlighted by the high angular deviation from the direction of the  
546 band (Fig. 12a). In medium-displacement deformation band, grains have a marked  
547 preferred orientation, both parallel and at 50-60° clockwise from the direction of  
548 deformation band (Fig. 12b). Grains in high-displacement deformation band are strongly  
549 aligned along the band direction and the most frequent angular classes fall within 40°

550 counter-clockwise and 10° clockwise direction to the reference deformation band plane  
551 (Fig. 12c). Grain preferential orientation in black gouge is well evident, with the majority of  
552 grain major axes falling within a 35° counter-clockwise angular fan from the gouge layer  
553 direction (Fig. 12d). Subsidiary fault has most of the grains preferentially oriented at 30-35°  
554 clockwise from the fault (Fig. 12e). Increasing displacement magnitude produces a more  
555 evident grain preferential orientation, with particles paralleling the direction of the  
556 deformation element.

557

## 558 **9. Discussion**

### 559 *9.1. Deformation mechanisms (particulate flow followed by cataclasis)*

560 In Figure 13, are summarized the main structural, microstructural and petrophysical  
561 properties of deformation features documented in the Rocca di Neto fault zone. The  
562 studied fault developed at very shallow-burial depth as indicated by stratigraphic  
563 constraints (Zecchin et al., 2012) and by the very weak compaction shown by the  
564 undeformed high-porosity sandstone, collectively suggesting a maximum burial depth  
565 below 400-500 m (Paxton et al., 2002). In this framework, deformation bands with  
566 displacement < 1 cm (Fig. 3a), characterized by grain re-organization and little grain size  
567 reduction, are interpreted to develop by particulate flow in highly porous sandstone (e.g.,  
568 Rawling and Goodwin, 2003; Balsamo and Storti, 2010; Rodrigues and Alves da Silva,  
569 2018) (Figs. 4b and 13a). Particulate flow does not obliterate the original texture of pristine  
570 sandstone, but rather operates a re-organization of fabric leading to a closer packing of  
571 grains and to porosity reduction, increasing contacts between particles (Antonellini et al.,  
572 1994; Kaproth et al., 2010; Soliva et al., 2013; Griffiths et al., 2016) (Figs. 7d and 13a). In  
573 low-displacement deformation bands within the low-deformation domain, the difference  
574 between the shape descriptors of deformed and undeformed domains is less pronounced



575 compared to the other deformation structures (Fig. 10a, b, c). This line of evidence  
576 supports particulate flow as the main deformation mechanism, causing very limited grain  
577 fragmentation throughout all the investigated size classes. Moving toward the master fault,  
578 deformation bands in the footwall damage zone show a more severe reduction of grain  
579 size, even for bands with few cm of displacement (Fig. 4c, d). Grains are internally  
580 fractured, indicating that cataclasis was the main deformation mechanism (Engelder, 1974;  
581 Aydin and Johnson, 1978; Blenkinsop, 1991; Balsamo and Storti, 2010) (Figs. 5a, b and  
582 13b, c). Grain breakage leads to a pronounced reduction of interparticle porosity (Fig. 7d),  
583 due to the presence of small grain fragments filling pores (Antonellini et al., 1994; Kaproth  
584 et al., 2010; Skurtveit et al., 2013; Torabi, 2014). The interpretation of a cataclastic  
585 deformation mechanism is also supported by the significant difference of the shape  
586 parameters of the three main mineralogical phases involved in the deformation, with quartz  
587 grains resulting more elongated and angular with respect to feldspar and lithic grains (Fig.  
588 11a, b, c). The difference of the shape descriptors is related to the development of grain-  
589 scale fractures produced by cataclastic processes involving the high-porosity sandstone  
590 (grain crushing, translation and rotation) (Balsamo and Storti, 2011; Skurtveit et al., 2013).  
591 Cataclasis is even more severe in high-displacement deformation bands inside the mixed  
592 zone and fault core, leading to the formation of a thin core with strongly comminute grain  
593 size and an ultra fine-grained matrix (Figs. 4d and 13d). The strongest degree of cataclasis  
594 is found in black gouges and in the fault core of subsidiary faults, where strain-localization  
595 is testified by the occurrence of ultra-comminute layers (Engelder, 1974; Mair et al., 2002b;  
596 Balsamo et al., 2014) (Figs. 4e, f and 13e, f). Microstructural observations, in conjunction  
597 with grain size and porosity data, suggest that particulate flow was active for displacement  
598 < 1 cm, whereas cataclasis settled for displacement > 1 cm and after a porosity loss to 5-  
599 6%. As highlighted by other authors, porosity exerts a strong control upon the deformation

600 mechanism affecting porous granular materials (Flodin et al., 2003; Shipton et al., 2005;  
601 Schultz et al., 2010).

602 In the investigated high-porosity sandstone, a porosity value of 5-6% can be assumed as  
603 the critical threshold to switch from particulate flow to cataclasis. Below this threshold,  
604 grains are forced to deform mostly via intragranular fracturing and then by abrasion during  
605 rolling (Fig. 5a, b).

606 The fragmentation of grains via cataclasis, promotes the development of more equant,  
607 smoother and regular shaped grains compared to the undeformed sandstone (Blenkinsop,  
608 1991; Heilbronner and Keulen, 2006; Storti et al., 2007; Balsamo and Storti, 2011) (Fig.  
609 11a, b, c). Grain shape data indicate that cataclasis acted selectively according to the  
610 mineralogy of grains. This is evident considering the systematically higher aspect ratio and  
611 lower circularity and solidity values shown by quartz with respect to feldspar, especially in  
612 the finer grain size range (Fig. 11). This difference in deformation mechanism can be  
613 linked to the presence of cleavages and twinning planes along the crystal structure of  
614 feldspar, acting as preferential breakage surfaces (Exner and Tschegg, 2012; Nicchio et  
615 al., 2018; Del Sole and Antonellini, 2019) (Figs. 5b and 14). The presence of the  
616 aforementioned reticular weaknesses, promotes the development of intragranular fractures  
617 during incipient cataclasis, leading to the formation of several equant small-sized clasts  
618 (Antonellini et al., 1994; Kaproth et al., 2010; Balsamo and Storti, 2011) (Fig. 14b, c).  
619 Quartz grains are less sensitive to the development of intragranular fractures due to the  
620 lack of twinning planes and to a higher hardness compared to feldspar. This results in  
621 deformation achieved mainly by grain splitting and abrasion of the asperities, and  
622 subordinately by intragranular fractures, forming highly elongated finer, and more equant  
623 smoothed coarse grains (cf. Balsamo and Storti, 2011) (Fig. 14d). Lithic fragments deform  
624 both via intragranular, trans-granular fracturing as well as by abrasion (Fig. 14b, c).

625 However, the deformation mechanism affecting lithics vary according to grain mineralogy  
626 (micas, gneiss-granitic fragments, bioclasts).

## 627 *9.2. Displacement-dependent cataclasis*

628 The deformation intensity in studied sub-seismic scale structures is related to the total  
629 amount of displacement accommodated by each deformation element. The investigated  
630 deforming structures display a different maturity of cataclastic fabric with increasing  
631 displacement (Figs. 4 and 6). In particular, in low-to medium-displacement deformation  
632 bands cataclasis is rather immature as testified by the slight decrease of mean grain size  
633 and sorting (Figs. 7a, b and 8a-f). High-displacement deformation bands and fault core of  
634 subsidiary faults accommodating higher offset are characterized by a more mature  
635 cataclastic fabric as indicated by the pronounced grain size reduction and widening of  
636 granulometric curves (i.e., sorting decrease) (Figs. 4d, f and 7a, b). Black gouges inside  
637 the fault core are interpreted as the products of extreme cataclasis caused by strain-  
638 localization, leading to the formation of thin, ultra-comminute layers (Fig. 4e). The  
639 increasing cataclastic intensity with displacement can be inferred also from the shape  
640 parameters of grains, in particular by evaluating the difference between quartz and  
641 feldspar (Fig. 11). Pronounced cataclasis is also responsible for the development of a  
642 weak foliation, imparted by the preferential alignment of grains parallel or at low-angle to  
643 the orientation of the deformation bands and gouges (Cladouhos, 1999; Cashman and  
644 Cashman, 2000) (Fig. 12). In summary, the higher is the accommodated displacement, the  
645 strongest is the foliation with major axis of grains paralleling the direction of the  
646 deformation element.

647 At the micro-scale, grain comminution is not uniform within the deformation band, but it is  
648 commonly more intense near one of the boundaries. This asymmetry of grain size  
649 comminution is caused by progressive localization of deformation on one side of the band

650 or gouge (Fig. 6b, c). The greater is the displacement, the stronger is the grain size  
651 reduction and the asymmetry of comminution within the deformation band, up to the  
652 development of a 100-200  $\mu\text{m}$ -thick slip surface (Figs. 4d). We suggest that the strain-  
653 localization on one side of the deformation bands could be caused by the kinematic stress  
654 field active in the vicinity of the master fault (Pizzati et al., 2019). This is further confirmed  
655 by the occurrence of microstructural asymmetry only inside deformation features close to  
656 the master fault, where the additional stress field was stronger.

657 Field observations indicate that deformation bands, subsidiary faults and gouges in the  
658 studied fault zone tend to increase their displacement approaching the master fault surface  
659 (Figs. 2 and 3). This is in accordance with the increase of the maturity of cataclastic fabric  
660 (Figs. 4 and 6), and also with the progressive increase of sorting-span and D-value with  
661 higher displacement magnitudes (Figs. 7 and 8). Inside the mixed zone and fault core, the  
662 presence of high-displacement structures (with offset exceeding bedding thickness)  
663 favored also the grain-scale mixing of layers with different grain size. Tectonic mixing is a  
664 common process in thinly-bedded siliciclastic successions (Heynekamp et al., 1999;  
665 Rawling and Goodwin, 2006; Balsamo and Storti, 2011). In the studied fault zone, tectonic  
666 mixing is testified by the anomalous coarser grain size in cores of subsidiary faults with  
667 respect to the surrounding foliated very fine sand (Fig. 8j-l). A further evidence is provided  
668 by the shape descriptor values that do not follow the increasing displacement trend  
669 identified by the other deforming structures. This would suggest a mixing of sediment  
670 volumes with different grain size concealing the real effect of the high-displacement  
671 magnitude (Figs. 10 and 11).

672 In the studied fault zone, we documented deformation features showing severe cataclasis  
673 even if the host sandstone was buried at very shallow depth ( $< 400\text{-}500\text{ m}$ ) (Zecchin et al.,  
674 2012). Following this, although typically favored by significant overburden, we suggest that  
675 cataclastic processes in high-porosity sandstones, may occur not only in deep-burial

676 settings (2-3 Km) (Ballas et al., 2015; Fossen et al., 2017), but also at shallower depth.  
677 Our data show that the onset of cataclasis depends mainly on the total displacement  
678 magnitude and upon the evolution of petrophysical-textural properties of the sandstone in  
679 the early stages of deformation. Following this, deep burial conditions are not strictly  
680 necessary for the onset of cataclasis in high-porosity arkosic to lithic arkosic sandstones.

### 681 *9.3. Displacement-dependent petrophysical properties*

682 The deformation mechanism previously described causes a strong deterioration of  
683 petrophysical properties of faulted sandstone, as underlined by the permeability drop  
684 characterizing the most deformed domains (exceeding four orders of magnitude  
685 diminishing) (Figs. 7c and 15). From cross-correlation graphs between permeability and  
686 petrophysical-textural properties it is possible to verify the role of each parameter in  
687 causing overall permeability decrement (Fig. 15). In particular, permeability shows a  
688 progressive decrease with increasing displacement from deformation bands to black  
689 gouges and subsidiary faults. Permeability vs 2-D porosity relationship describes a linear  
690 decreasing trend with increasing displacement (Fig. 15a). Conversely, permeability vs  
691 grain size is best fitted by a power-law function, with finer grain size (higher displacement)  
692 correlating with lowest permeability values (Fig. 15b). Permeability vs sorting-span is again  
693 fitted by a power-law distribution, but with negative exponent. Grain size distribution curves  
694 with high span (wide curves) are related with the lowest permeability values (Fig. 15c).  
695 Thus, a decrease of 2-D porosity and grain size and at the same time span increase  
696 (sorting decrease) due to cataclasis in response to incremental displacement, strongly  
697 affect the permeability drop of faulted sandstone. From the three graphs is evident the  
698 anomalous values reported for the subsidiary fault, not following the displacement  
699 relationship described by the other structural elements (Fig. 15a, b, c). This discrepancy  
700 can be interpreted as a further evidence for tectonic mixing affecting deformation features

701 with displacement exceeding sedimentary bed thickness (Heynekamp et al., 1999;  
702 Rawling and Goodwin, 2006). This implies that porosity as well as grain size and span  
703 data are the results of deformation mechanism (cataclasis) and mixing of sediments with  
704 different textural and petrophysical properties.

705 The influence of grain shape (aspect ratio, circularity and solidity) in determining the  
706 permeability drop was also checked (Fig. 15d, e, f). Cumulative data indicate that lower  
707 permeability values are associated with slightly lower aspect ratio (equant grains)  
708 characterizing deformed particles (Fig. 15d). Deformed domains with lower permeability  
709 show also higher circularity (circle-shaped grains) (Fig. 15e). Significant permeability drop  
710 is associated with higher particle solidity (smoother grains) (Fig. 15f). Although shape  
711 descriptors of undeformed and deformed sandstone display different values, differences  
712 are not so pronounced. This can be translated in a minor role played by the development  
713 of more equant, regular and smoothed particles via cataclasis to the overall permeability  
714 decrease (Fig. 15d, e, f). Following this, from the shown datasets we interpret 2-D porosity,  
715 grain size and sorting-span as the main drivers for permeability drop occurring with  
716 increasing displacement.

#### 717 *9.4. Implications for fluid flow*

718 The deformation mechanism previously described causes a deterioration of petrophysical  
719 properties of the faulted sandstone following the increase of displacement. Even  
720 deformation bands with low-displacement ( $< 1$  cm), accommodated dominantly via  
721 particulate flow, may show a permeability drop of at least half an order of magnitude (Fig.  
722 16a). Deformation bands with higher displacement ( $1 \text{ cm} < d < 5 \text{ cm}$ ), developing an  
723 immature cataclastic fabric, may induce a permeability decrease up to 1.5 orders of  
724 magnitude (Fig. 16b). High-displacement bands ( $5 \text{ cm} < d < 10 \text{ cm}$ ) feature an effective  
725 permeability drop from 2 to 3 orders of magnitude, due to the pronounced cataclastic fabric

726 formed via intense fragmentation followed by abrasion of grains during rolling and  
727 translation (Fig. 16c). In these bands, strain-localization may occur along the boundary  
728 between band and undeformed sand thus leading to a gradient of porosity and  
729 permeability drop approaching the preferential slip surface (Figs. 9 and 16c). Mature  
730 cataclasis affecting the core of subsidiary faults ( $d > 20$  cm) and gouges ( $d \sim 15$  cm)  
731 causes a drop of mean permeability up to 4 orders of magnitude due to extreme grain size  
732 reduction and to the highest measured span of the granulometric curves (Fig. 16d).  
733 Therefore, early stage particulate flow followed by cataclasis affecting poorly lithified  
734 sandstone can reduce the effective permeability up to 4 orders of magnitude even with  
735 moderate displacement (10-20 cm). Following this, displacement is a key factor in  
736 controlling the permeability of sub-seismic deformation structures developed in high-  
737 porosity rocks, in conjunction with burial depth and stress-strain conditions (Ballas et al.,  
738 2012, 2015).

739 The studied deformation features are likely to have played a barrier role toward fluids  
740 orthogonal to the strike of the structural elements (Fig. 7). However, the real influence  
741 upon fluid flow has to be related to the lateral continuity and three-dimensional  
742 arrangement of deformation bands and gouges (Shipton et al., 2005; Sternlof et al., 2006;  
743 Kolyukhin et al., 2010; Ballas et al., 2015). Moreover, lateral variations concerning  
744 thickness of deformation bands can be a critical parameter in decreasing the sealing  
745 potential at the scale of the single band (Rotevatn et al., 2013, 2017).

746 The presence of deformed whitish sand within deformation bands, surrounded by orange-  
747 brown stained undeformed sandstone due to iron oxide precipitation, suggests an effective  
748 sealing behavior even for a few cm displacement (Fig. 3a). Even though, the barrier-conduit  
749 role within deformed high-porosity sandstone is not straightforward as it is in the case of  
750 fully lithified rocks (Caine et al., 1996; Evans et al., 1997; Fisher et al., 2018). Whereas in  
751 lithified rocks the fault core acts as an effective barrier and the damage zone as a

752 preferential conduit, in granular materials the sealing behavior may depend on the  
753 hydrological conditions (Sigda and Wilson, 2003; Wilson et al., 2003; Balsamo et al.,  
754 2012). In water-saturated conditions deformation bands and gouges display a barrier role,  
755 while in unsaturated ones, they may act as partial conduits due to high retention time of  
756 fluids within the deformed sediments (Sigda and Wilson, 2003). The Rocca di Neto fault  
757 zone has a present-day barrier role (as testified by *in situ* permeability measurement) (Fig.  
758 7c), while during the early stages of deformation, the partial conduit behavior is witnessed  
759 by the presence of selective cementation along deformation bands and faults (Balsamo et  
760 al., 2012; Pizzati et al., 2019). This change in hydrological behavior is likely related to the  
761 different diagenetic environments and water-saturation conditions experienced by the fault  
762 during the deformation history and basin-scale tectonic exhumation occurred since Middle  
763 Pleistocene.

764 Our results could be useful to evaluate the possible compartmentalization of high-porosity  
765 sandstone reservoirs deformed at shallow-burial depth, through development of sub-  
766 seismic deformation structures (deformation bands and gouges). Such deformation  
767 features may represent major hydraulic discontinuities even after few cm of  
768 accommodated displacement.

769

## 770 **10. Conclusions**

771 We described the meso-scale structural features, microstructural characteristics and  
772 petrophysical properties of the extensional Rocca di Neto fault zone, deforming lithic  
773 arkosic to arkosic poorly lithified shoreface sandstones. Deformation occurred at shallow-  
774 burial conditions (< 400-500 m) and the pristine sandstone was characterized by high  
775 primary porosity. On the basis of our observations we came to the following main  
776 conclusions:



777 1- The deformation mechanisms responsible for the development of deformation bands  
778 are non-destructive particulate flow followed by cataclasis. Cataclasis becomes dominant  
779 after porosity decrease to 5-6%, and is more intense with increasing displacement  
780 eventually forming black gouges in the fault core, characterized by extreme grain size  
781 reduction, poor sorting and high D-value.

782 2- Cataclasis acts differently according to the mineralogy of the deformed grains: feldspar  
783 grains deform mainly by intragranular fractures leading to several equant sub-grains with  
784 circular and more regular shape, while quartz grains are less affected by intragranular  
785 fractures and deform by flaking of asperities producing more elongated chips. Thus, the  
786 resulting quartz clasts are more elongated, less circular and less smooth with respect to  
787 feldspar ones at finer grain size, while the difference is less pronounced at coarser grain  
788 size range.

789 3- The intensity of cataclasis is more pronounced along deformation bands, subsidiary  
790 faults and black gouges accommodating high offset. At the scale of the whole fault zone,  
791 deforming structures are characterized by an increasing displacement gradient  
792 approaching the master fault surface. In high-strain structural domains (mixed zone and  
793 fault core) cataclasis along high-displacement structures is accompanied by tectonic  
794 mixing of sediments having different grain size.

795 4- In deformation bands and gouges, the grain size is drastically reduced (7-8 times) with  
796 respect to the pristine sandstone, and permeability shows drops up to 3-4 orders of  
797 magnitude, in agreement with the total displacement accommodated along single  
798 structures. Permeability decreases as a function of displacement, coupled with grain size  
799 and porosity diminishing and span increase (sorting decrease). Conversely, evolution of

800 grain shape played a minor role in determining the magnitude of permeability drop  
801 associated with deformed domains.

802 5- Cataclasis-related sub-seismic deformation structures (deformation bands and gouges)  
803 developing in high-porosity sandstones are capable of locally compartmentalize reservoirs  
804 deformed at shallow-burial depth. The occurrence of cataclastic processes at very shallow-  
805 burial conditions is related to major extent to the evolution of petrophysical and textural  
806 properties of deformed sandstone following increasing displacement magnitude.

807

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823

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- 1115

1116 **Figure captions**

1117 **Fig. 1.** (a) Geographic position of the Crotona Basin in the framework of the Southern  
1118 Apennine orogenic belt and Calabrian Arc. The thinly dotted line marks the landward limit  
1119 of the on-shore portion of the Crotona Basin. (b) Simplified geological map of the Crotona  
1120 Basin with the position of the study area along the extensional fault system affecting the  
1121 middle sector of the basin (modified after Zecchin et al., 2003). (c) Detailed geological  
1122 cross-section of the study area reporting the position of the Rocca di Neto fault zone  
1123 (redrawn after Balsamo et al., 2012). The trace of the cross-section is indicated by the  
1124 black and white star in Fig. 1b. ATB, Apennine thrust belt; CA, Calabrian Arc; CAW,  
1125 Calabrian accretionary wedge; CB, Crotona Basin.

1126 **Fig. 2.** Architecture and structural data of the studied fault zone (adapted from Pizzati et  
1127 al., 2019). (a) Detailed geological cross-section through the footwall of the Rocca di Neto  
1128 fault, developing inside the Early Pleistocene Scandale poorly lithified sandstone. The  
1129 hanging wall is almost completely covered by vegetation and debris and hosts the Middle  
1130 Pleistocene Cutro Clay. The blue dots along the fault zone represent the 68 permeability  
1131 and grain size sampling-measuring sites. Dotted rectangles report the exact position of the  
1132 photographs shown in Fig. 3. (b) Cumulative structural data of faults and deformation  
1133 bands also reporting the extensional slickenlines (Schmidt equal area, lower hemisphere  
1134 projection). The three mean planes of the identified deformation band sets are calculated  
1135 from the contour of poles to deformation bands. Stereonets were realized with  
1136 Allmendinger's "*Stereonet 10.0 software*" (Cardozo and Allmendinger, 2013). (c) Sketch  
1137 illustrating the most recurrent deformation structures along the studied fault zone. DB<sub>1</sub>,  
1138 synthetic high-angle deformation band; DB<sub>2</sub>, antithetic low-angle deformation band; DB<sub>//</sub>,  
1139 fault-parallel deformation band; SF, subsidiary fault; MF, master fault; FMZ, footwall mixed

1140 zone; FC, fault core; c.i., contouring interval; n, number of measured faults and  
1141 deformation bands

1142 **Fig. 3.** Outcrop details of the main deformation elements. (a) Low-displacement  
1143 deformation band ( $d < 1$  cm), inside the low-deformation domain. See the whitish color of  
1144 deformed sandstone within the band contrasting with the marked orange-colored oxidation  
1145 front abutting at the contact with the outer part of the band (black arrows). (b) Conjugate  
1146 deformation bands characterizing the footwall damage zone of the fault, organized in two  
1147 distinct sets, synthetic high-angle ( $DB_1$ ) and antithetic low-angle ( $DB_2$ ) with respect to the  
1148 master fault. A third set is composed of deformation bands parallel to subsidiary faults  
1149 ( $DB_{//}$ ). See the coin in the top left corner of the image for scale. (c) High-strain deformation  
1150 band surrounding a subsidiary fault hosted at the boundary between the footwall damage  
1151 zone and the mixed zone. The fault is selectively cemented via precipitation of calcite  
1152 cement (CC) (see the coin for scale). (d) Black gouges inside the fault core encased by  
1153 mixed coarse and fine foliated sand (pencil for scale).  $DB_1$ , synthetic high-angle  
1154 deformation band;  $DB_2$ , antithetic low-angle deformation band;  $DB_{//}$ , fault-parallel  
1155 deformation band; CC, carbonate concretion.

1156 **Fig. 4.** (a) Ternary Quartz-Feldspar-Lithics diagram showing the modal composition of the  
1157 pristine sandstone, following the classification of Folk (1974). Sediment composition was  
1158 measured on 35 different petrographic images evaluating the percentage of the dominant  
1159 mineralogical phases. Plane-polarized photomicrographs of microstructural features of  
1160 deformation bands and gouges. (b) Low-displacement fault-parallel deformation band  
1161 within the low-deformation zone showing grain re-orientation and limited fragmentation. (c)  
1162 Fault-parallel deformation band ( $DB_{//}$ ) within the footwall damage zone displaying  
1163 pronounced grain size reduction. Coarse grains are surrounded by a fine-grained light-  
1164 brown matrix formed by highly comminute fragments. (d) High-displacement fault-parallel

1165 deformation band close to the master fault, with a well developed ultra-comminute central  
1166 core showing brownish matrix and an outer part with less pronounced grain size reduction.  
1167 Tiny tensile fractures may develop both parallel and inclined to the band direction (white  
1168 arrows). (e) Thin black gouge with severe comminution of grains in localized shear zone  
1169 and S-C type structures imparted by the alignment of survivor grains and clay minerals. (f)  
1170 Fault core of a subsidiary fault with cataclastic fabric, given by highly heterogeneous grain  
1171 size distribution and poor sorting. DB, deformation band; Q, quartz; F, K-feldspar; L, lithic  
1172 fragment.

1173 **Fig. 5.** Detailed plane-polarized photomicrographs of the grain-scale deformation features.  
1174 (a) Pervasive crushing of lithic fragments and feldspar grains by intragranular and trans-  
1175 granular fractures, in the outer part of a low-displacement band. Porosity of this sample is  
1176 still high due to the lack of fine-grained matrix produced after severe grain crushing  
1177 following higher displacement magnitude. (b) Details of intragranular fractures affecting  
1178 feldspar, developed along crystal twinning planes, and flaking of asperities characterizing  
1179 quartz grains. Pores are partially filled by a fine-grained matrix formed by quartz chips and  
1180 feldspar fragments. (c) Oversized survivor feldspar grain in a medium-displacement band.  
1181 The brown matrix is composed of fine-grained quartz, feldspar and calcite flakes. (d)  
1182 Survivor grains of quartz inside a high-displacement deformation band, are not affected by  
1183 fracturing or flaking. Qz, quartz; K-f, K-feldspar; L, lithic fragment; P, pore space.

1184 **Fig. 6.** Back-scattered SEM photomicrographs of deformation bands and gouges. (a)  
1185 Medium-displacement deformation band with grains, especially feldspar, affected by  
1186 intragranular fractures in its outer part (white arrows). Conversely, inside the deformation  
1187 band itself grains rarely display fractures. (b) High-displacement deformation band close to  
1188 the fault core, displaying a central core with pronounced grain size reduction, developing a  
1189 slip surface on one side of the core. Grain size reduction has a decreasing gradient from

1190 the slip surface toward the other side of the band. This sample was selectively cemented  
1191 by calcite precipitation during progressive deformation. (c) Black gouge characterized by  
1192 extreme comminution along the slip zone and by a gradient of grain size reduction moving  
1193 away from it. Black gouge samples are often characterized by slip localization along the  
1194 hanging wall side. Qz, quartz; K-f, K-feldspar; L, lithic fragment; P, pore space; C, calcite  
1195 cement; M, biotite mica; SS, slip surface.

1196 **Fig. 7.** Inter-quartile box-whisker plots of petrophysical properties of the most recurrent  
1197 lithologies and deformation elements throughout the fault zone. (a) Mean grain size  
1198 obtained from the analyses performed with the laser granulometer. (b) Sorting-span of the  
1199 grain size distribution curves. (c) *In situ* air-permeability values measured with the Tiny  
1200 Perm II permeameter. (d) Two-dimensional porosity calculation from image analysis of thin  
1201 section photomicrographs. LDZ, low-deformation zone; FDZ, footwall damage zone; FMZ,  
1202 footwall mixed zone; FC, fault core; DB<sub>1</sub>, synthetic high-angle deformation band; DB<sub>2</sub>,  
1203 antithetic low-angle deformation band; n, number of measurements or analyses.

1204 **Fig. 8.** Comparison of grain size distribution curves, D-value (fractal dimension) and ratio  
1205 of faulted vs undeformed particles between sample pairs representative of the most  
1206 recurrent deformation features. Sample pairs were selected to directly compare deformed  
1207 structures with the surrounding host sediments. D-value provides details concerning the  
1208 cumulative particle number, indicating the number of fine vs coarse grains through a factor  
1209 describing the slope of the power-law function fitting data distribution. Ratio of particle  
1210 number between faulted and undeformed domains is useful to evaluate the relative  
1211 increase or decrease of particles in a specific grain size range. Red color is used to  
1212 distinguish deformed domains, while undeformed ones are reported in blue. (a, b, c) Low-  
1213 displacement deformation band vs undeformed medium-fine sand inside the low-  
1214 deformation zone. (d, e, f) Medium-displacement deformation band vs undeformed

1215 medium-fine sand inside the footwall damage zone. (g, h, i) High-displacement  
1216 deformation band vs undeformed medium-fine sand inside the footwall damage zone. (j, k,  
1217 l) Fault core of subsidiary fault vs foliated very fine sand inside the footwall mixed zone.  
1218 (m, n, o) Black gouge vs foliated very fine sand inside the fault core; GSD, grain size  
1219 distribution; DB, deformation band;  $\Phi$ , mean grain size; d, displacement.

1220 **Fig. 9.** Plane-polarized photo-mosaics reporting the porosity variation across low-  
1221 displacement band (a), medium-displacement band (b) and black gouge (c). Two-  
1222 dimensional porosity is reported on profile crossing the entire length of the structural  
1223 element as mean percentage calculated from the areas delimited by white dotted lines  
1224 throughout the deformation structures.

1225 **Fig. 10.** Grain shape analysis performed on cumulative data of the most representative  
1226 deformation features: low, medium, high-displacement deformation bands, fault core of  
1227 subsidiary fault and black gouge. Grains are described using three shape descriptors,  
1228 aspect ratio (a), circularity (b) and solidity (c). Symbols represent mean values of the  
1229 shape parameters plotted as ratio between the faulted and undeformed samples, to ease  
1230 the recognition of differences and similarities between the five datasets. All data are  
1231 subdivided in five distinct grain size classes, 50  $\mu\text{m}$  each. Complete datasets are provided  
1232 in the online Supplementary material Figs. A7 and A8, together with data regarding the  
1233 undeformed medium-fine sand adopted as reference and statistical analysis. d,  
1234 displacement; n, number of grains traced and analyzed via image analysis.

1235 **Fig. 11.** Grain shape analysis performed on the three most recurred minerals (quartz,  
1236 feldspar and lithic fragments) in low, medium, high-displacement deformation bands, fault  
1237 core of subsidiary fault and black gouge. Grains are described using three shape  
1238 descriptors, aspect ratio (a), circularity (b) and solidity (c). Symbols represent mean values

1239 of the shape parameters plotted as ratio between the faulted and undeformed samples, to  
1240 ease the recognition of differences and similarities between the five datasets. All data are  
1241 subdivided in four distinct grain size classes, 50  $\mu\text{m}$  each; the coarser grain size class from  
1242 200 to 250  $\mu\text{m}$  was omitted because of the limited number of data unable to provide  
1243 statistical robustness. Complete datasets are provided in the online Supplementary  
1244 material Figs. A9 and A10, together with data regarding the undeformed medium-fine sand  
1245 adopted as reference and statistical analysis. Qz, quartz; K-f, feldspar; L, lithic fragment; d,  
1246 displacement; n, number of grains traced and analyzed via image analysis.

1247 **Fig. 12.** Half-rose plots of the preferential orientation of grains according to the angle  
1248 between the major axis and a horizontal reference plane. Undeformed control samples are  
1249 on the left side (green diagrams), while deformed counterparts are on the right side of the  
1250 figure (red diagrams). Preferential orientation for low-displacement (a), medium-  
1251 displacement (b), high-displacement deformation band (c), black gouge (d) and subsidiary  
1252 fault (e). Black dotted lines indicate the orientation of the deformation band, gouge or fault  
1253 on thin section. d, displacement; n, number of grains.

1254 **Fig. 13.** Microstructural features according to the identified deformation mechanism. (a)  
1255 Inside the low-deformation zone and the outer damage zone, deformation bands  
1256 accommodated small-scale displacement (typically < 5 cm). Along these structures  
1257 deformation is mainly achieved via particulate flow with fabric re-organization and  
1258 negligible grain fragmentation. This causes a decrease of porosity from 37% of the pristine  
1259 sandstone to 5-7% within deformation bands. (b) In the outer footwall damage zone,  
1260 higher displacement along deformation bands forced grains, especially feldspar, to break  
1261 along crystal weaknesses such as twinning planes. Quartz is less affected by  
1262 fragmentation via intragranular fracturing and deforms mainly by flaking and chipping of  
1263 the asperities along the outer surface. (c) Inside the footwall damage zone, fault-parallel

1264 deformation bands with displacement above 5 cm, are characterized by an immature  
1265 cataclastic fabric, with grain size reduction and sorting diminishing. (d) High-displacement  
1266 deformation bands may develop an inner core with severe grain size reduction, leading to  
1267 the formation of a brownish matrix composed of crushed feldspar and calcite grains. To  
1268 the outer part of the band grain size reduction is less pronounced. Eventually, within the  
1269 mixed zone and fault core the most deformed end-members are located, with subsidiary  
1270 faults (e) displaying an asymmetric structure with a slip surface and a decreasing gradient  
1271 of grain size reduction moving away from it. Within the fault core, black gouges (f) display  
1272 extreme grain crushing leading to the formation of ultra-comminute thin layers, encased by  
1273 less deformed sand arranged in S-C arrays. The deformation mechanism described above  
1274 is able to reduce the permeability up to 3.5-4 orders of magnitude with respect to the  
1275 pristine high-porosity sandstone.  $K_{av}$ , average permeability; SS, slip surface; d,  
1276 displacement.

1277 **Fig. 14.** Grain-scale deformation mechanism. (a) Undeformed high-porosity sand. (b) Early  
1278 deformation with compaction leading to intragranular crushing of feldspar and flaking of  
1279 coarser quartz grains. Lithic fragments are affected by trans-granular as well as  
1280 intragranular fractures. (c) With progressive deformation, crushing of feldspar produces  
1281 sub-equant particles, while flakes of quartz grains display highly elongated shape with  
1282 angular borders. (d) In the final stage of deformation, cataclasis forms angular fine-grained  
1283 quartz flakes and equant-smooth fine-grained feldspar clasts. The oversized-survivor  
1284 quartz and feldspar clasts are more equant and display smooth shape. Qz, quartz; K-f,  
1285 feldspar; L, lithic grain; P, pore space.

1286 **Fig. 15.** Relationships between permeability ratio of faulted and undeformed sediments  
1287 with petrophysical properties and shape descriptors. (a) Permeability ratio vs 2-D porosity  
1288 calculated on thin section. (b) Permeability ratio vs mean grain size measured by laser

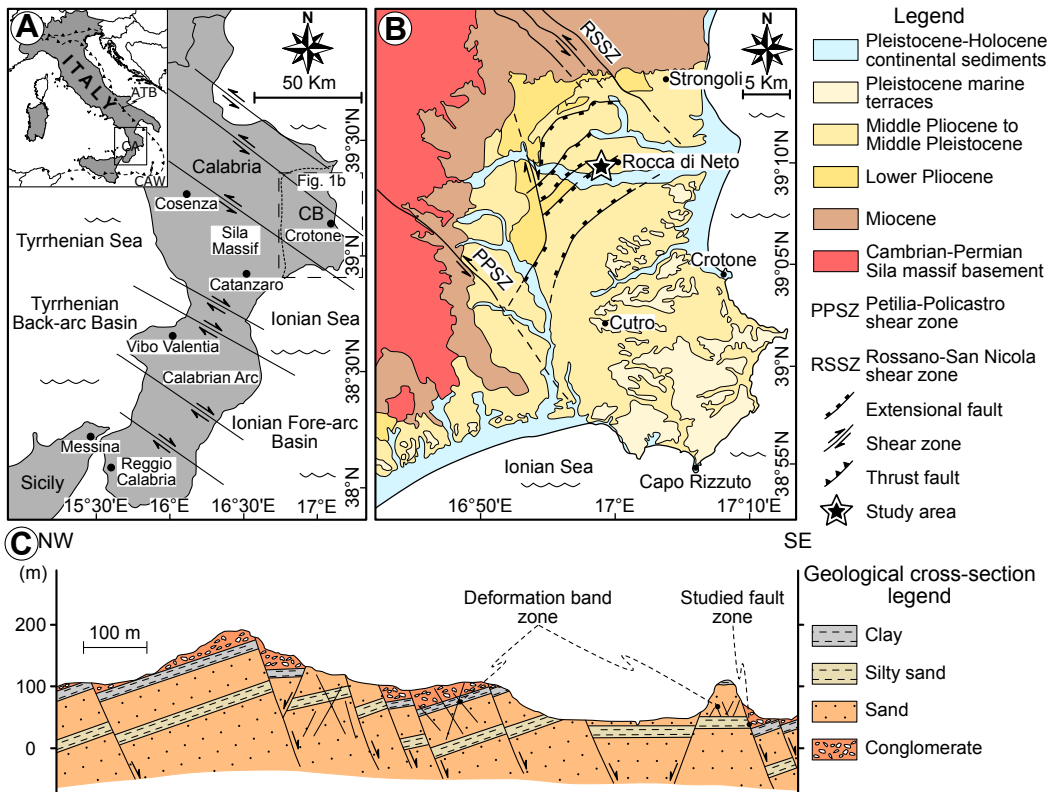


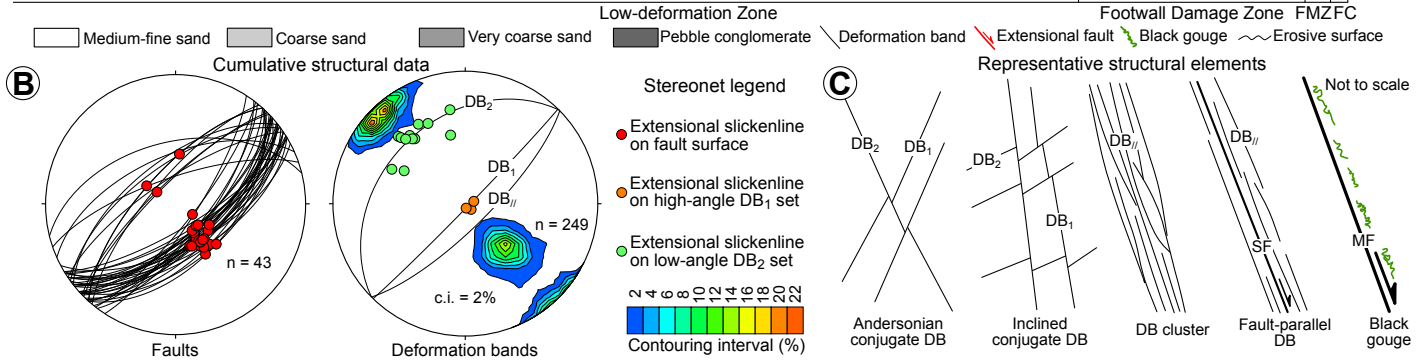
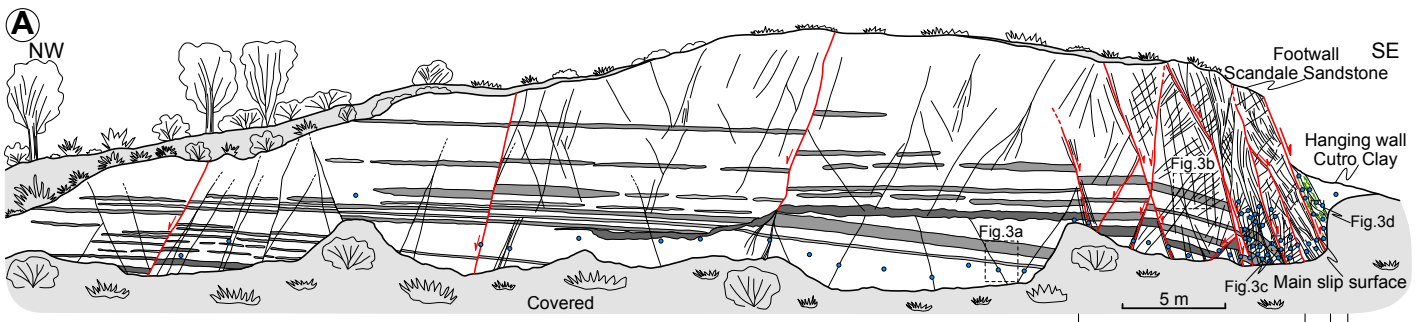
1289 diffraction. (c) Permeability ratio vs mean sorting-span gained from laser diffraction  
1290 analysis. (d) Permeability ratio vs grain aspect ratio from cumulative data. (e) Permeability  
1291 ratio vs grain circularity from cumulative data. (f) Permeability ratio vs grain solidity from  
1292 cumulative data. The reference permeability was assumed as a mean of all permeability  
1293 measurements on the undeformed sandstone outside the fault zone. Error bars represent  
1294 the standard deviation associated with datasets. d, displacement; n, number of  
1295 measurements, analysis and grains traced on thin section.

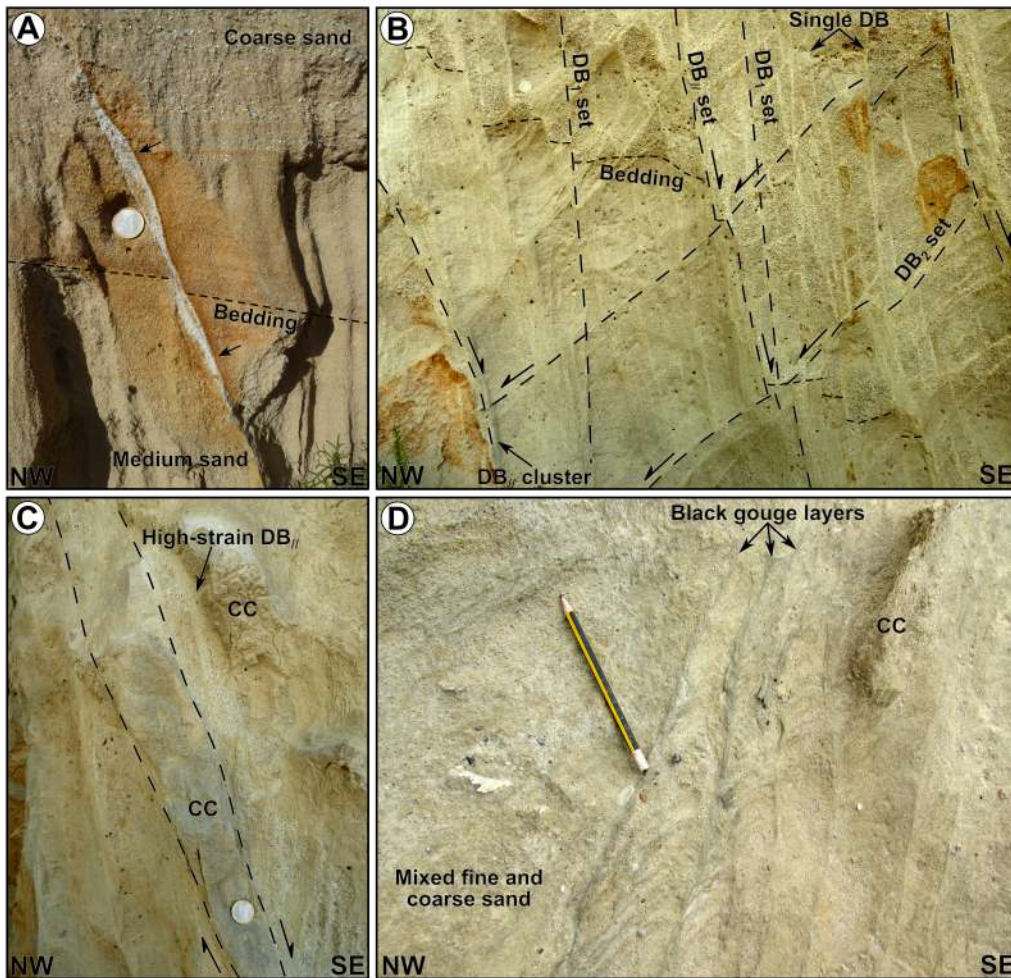
1296 **Fig. 16.** Evolutionary model of deforming structures from low-offset deformation bands to  
1297 faults. (a) Particulate flow affecting low-displacement deformation bands causes a weak  
1298 grain size reduction and a closer packing of grains, leading to mean porosity of 5-6%. The  
1299 reduction of porosity features a decrease of permeability of less than one order of  
1300 magnitude. (b) In medium-displacement deformation bands the onset of fragmentation and  
1301 rolling of grains results in an immature cataclastic fabric, responsible for the reduction of  
1302 grain size and sorting. Porosity is further reduced (2-3%) as well as permeability (1.5  
1303 orders of magnitude less than undeformed sand). (c) High-displacement deformation  
1304 bands are affected by pronounced cataclasis and strain-localization processes inducing an  
1305 asymmetrical drop of porosity (~ 1%) and permeability (3 orders of magnitude less than  
1306 the undeformed sandstone). (d) Eventually, along subsidiary faults with offset > 20 cm,  
1307 cataclasis is extreme and severe grain size reduction leads to low values of porosity (<  
1308 1%) and to a permeability contrast up to 4 orders of magnitude with respect to the pristine  
1309 sandstone.  $K_{\text{fault}}$ , average permeability of faulted sandstone;  $K_{\text{und}}$ , average permeability of  
1310 pristine sandstone; d, displacement.

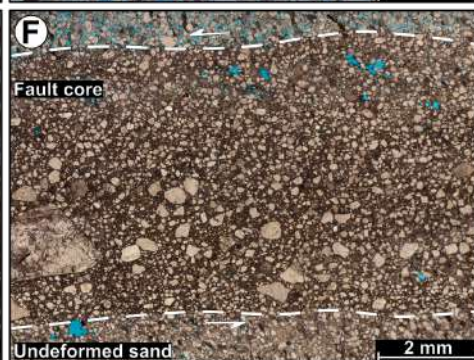
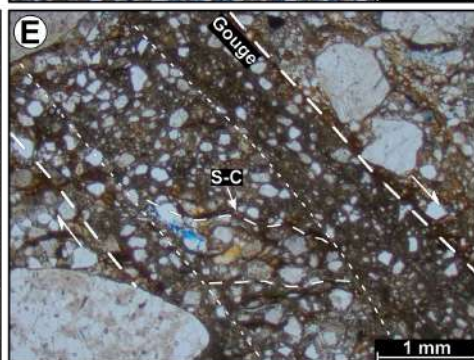
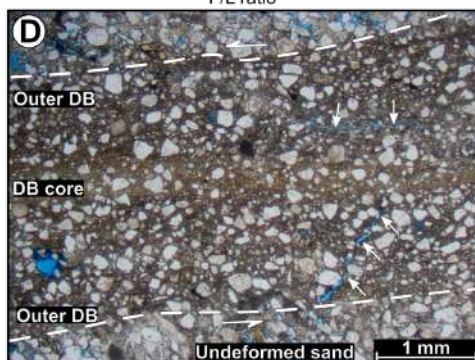
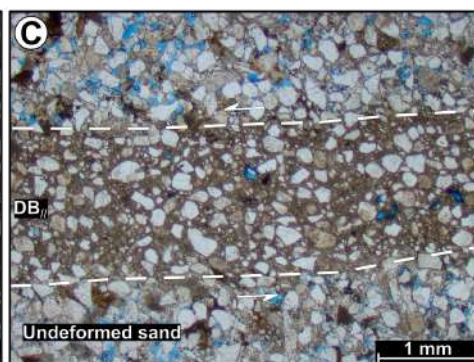
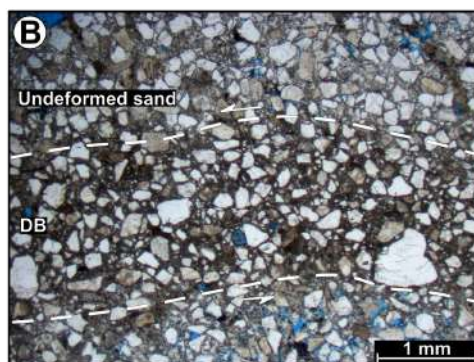
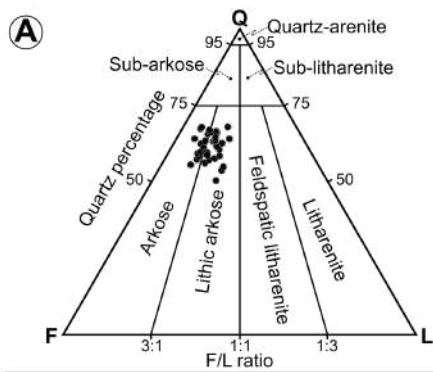
1311 **Table 1.** Structural position, deforming element, distance from the master fault, mean  
1312 diameter, mode, sorting-span (with associated standard deviation), D-value and  $R^2$  of the  
1313 analyzed grain size samples. LDZ, low-deformation zone; FDZ, footwall damage zone;

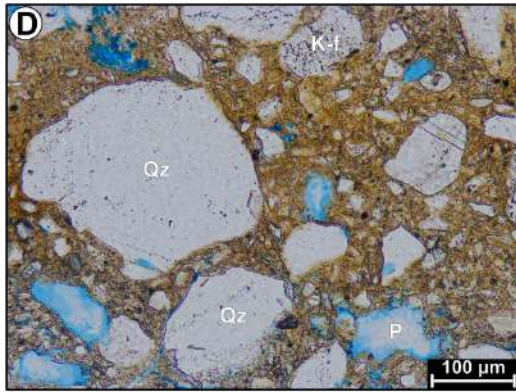
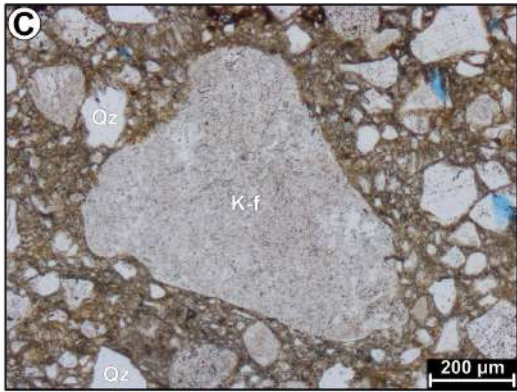
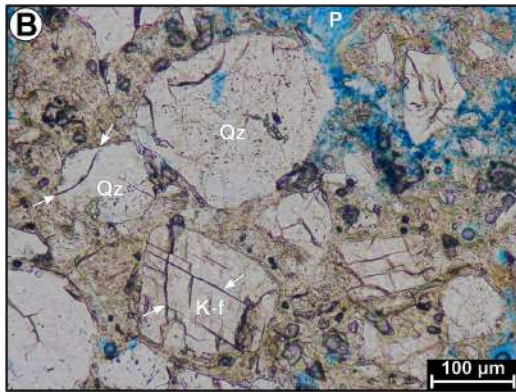
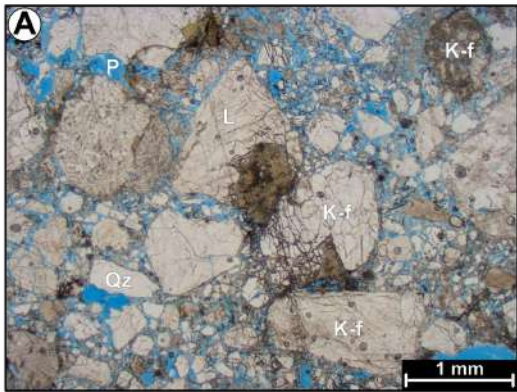
1314 FMZ, footwall mixed zone; FC, fault core; MF, master fault; DB<sub>1</sub>, synthetic high-angle  
1315 deformation band; DB<sub>2</sub>, antithetic low-angle deformation band.

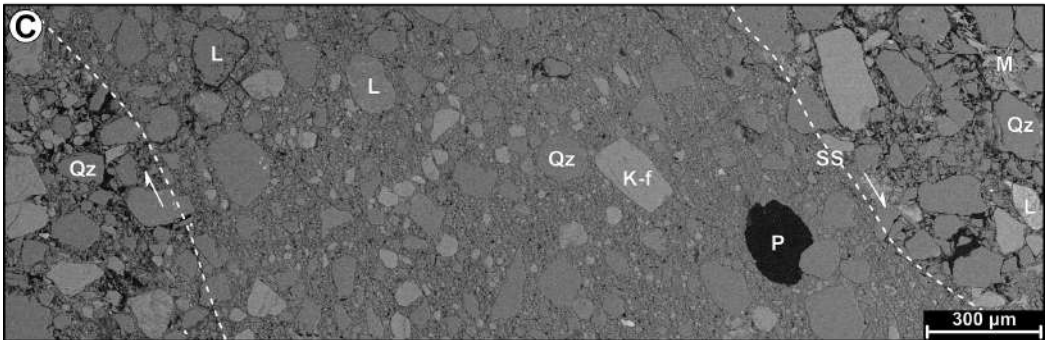
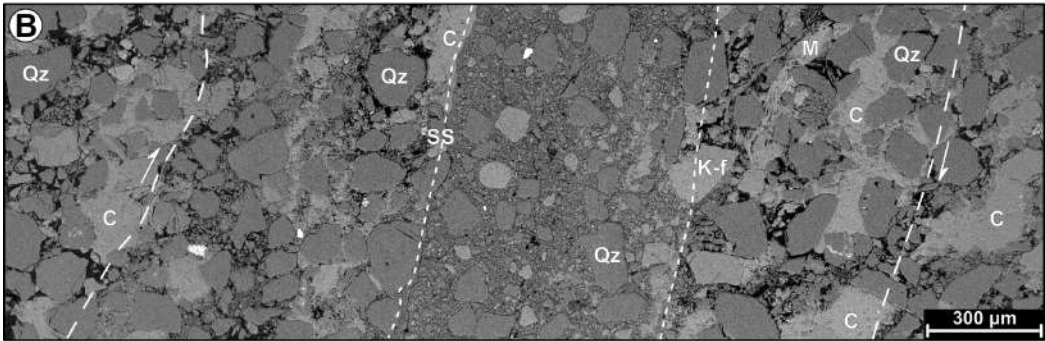
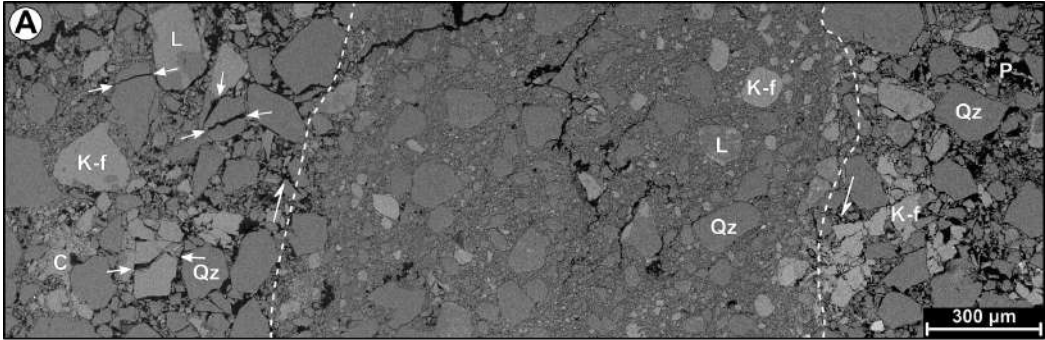




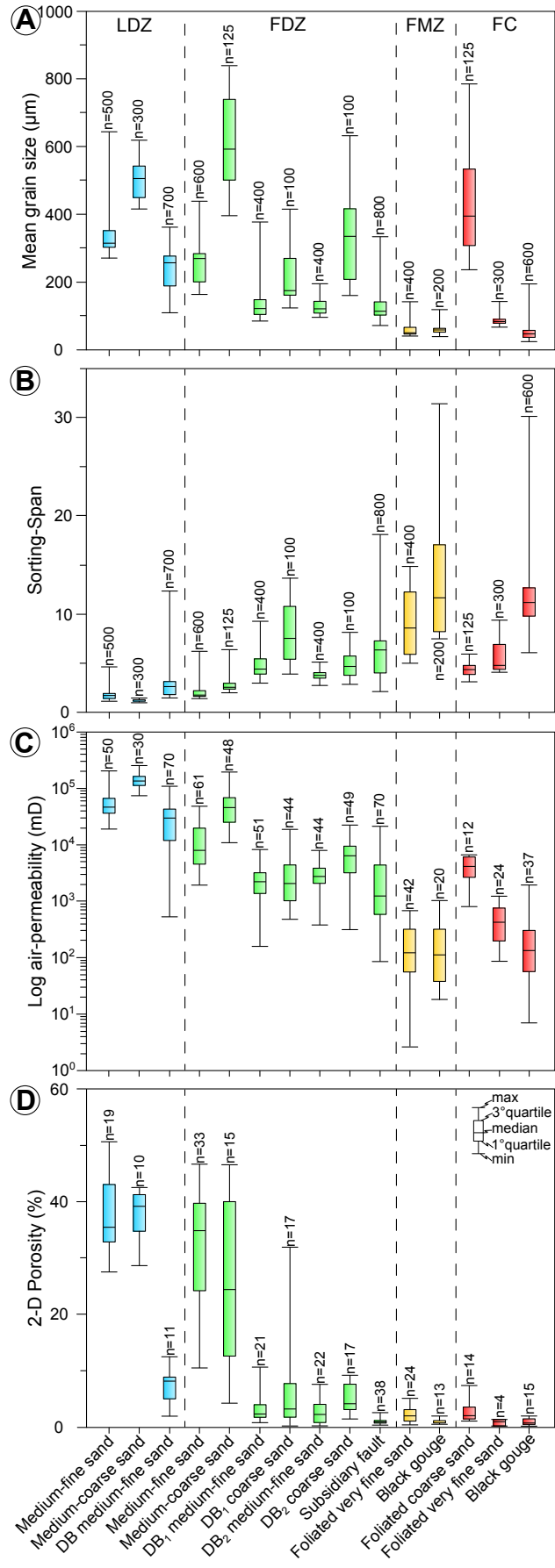


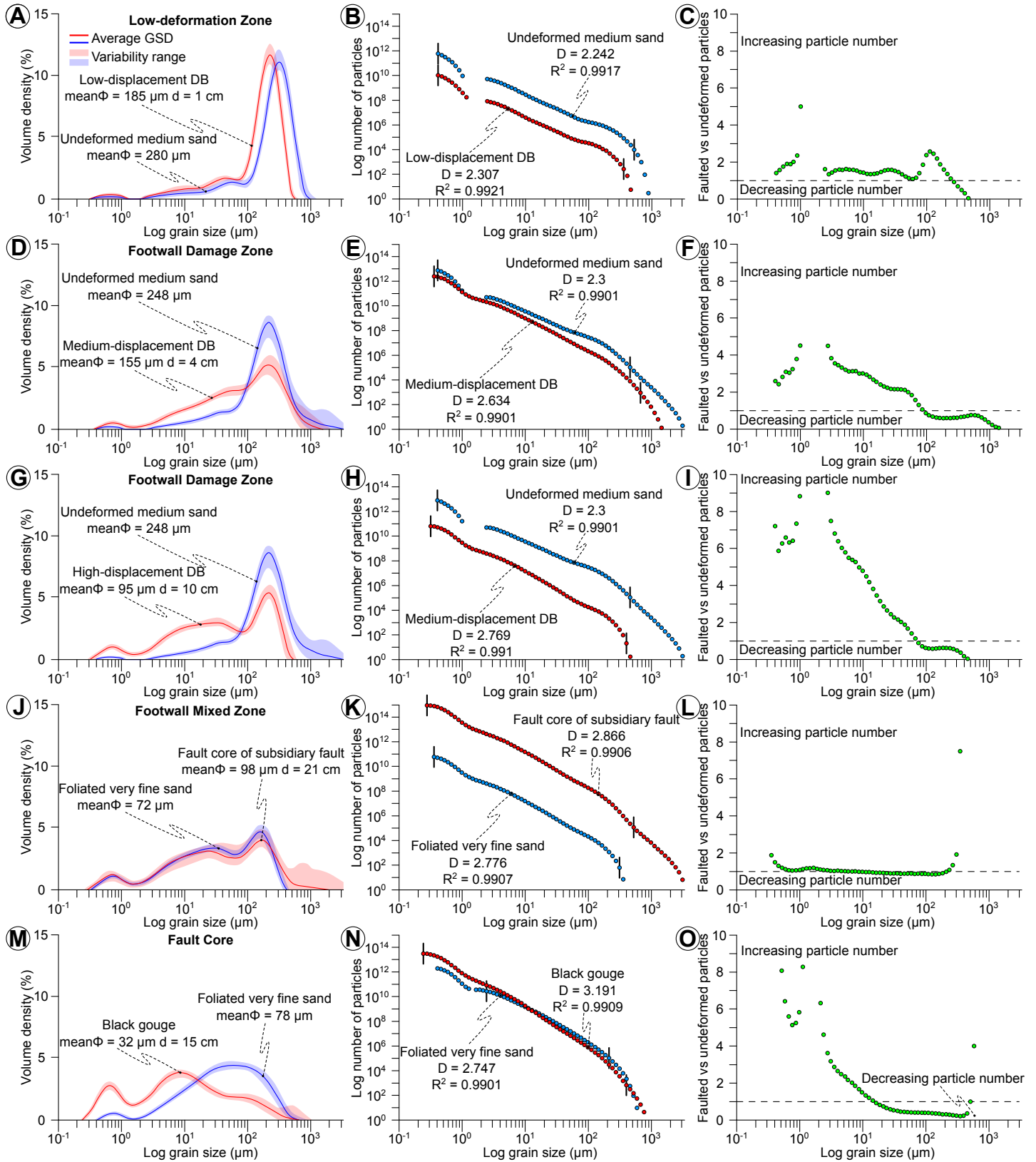


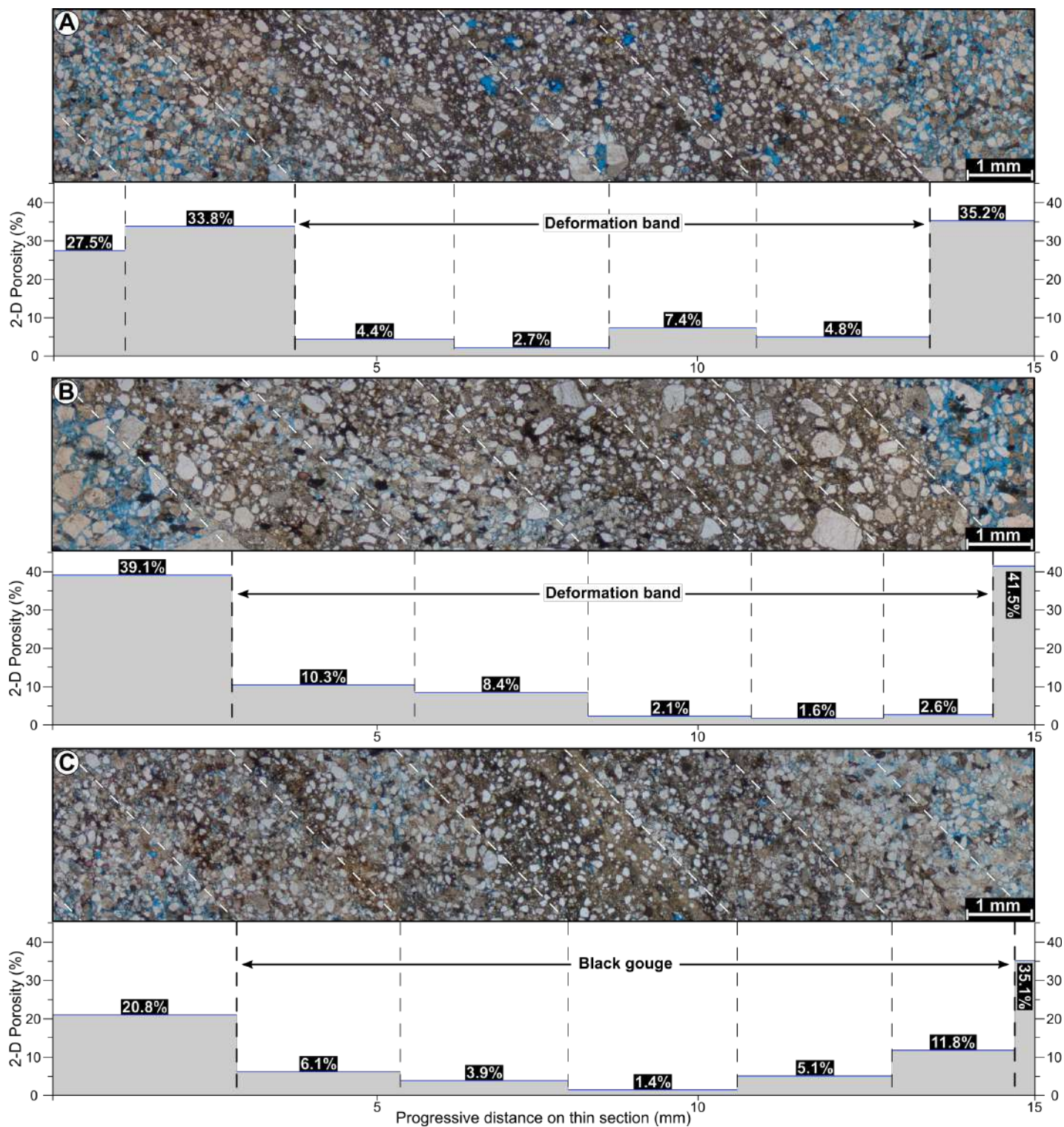


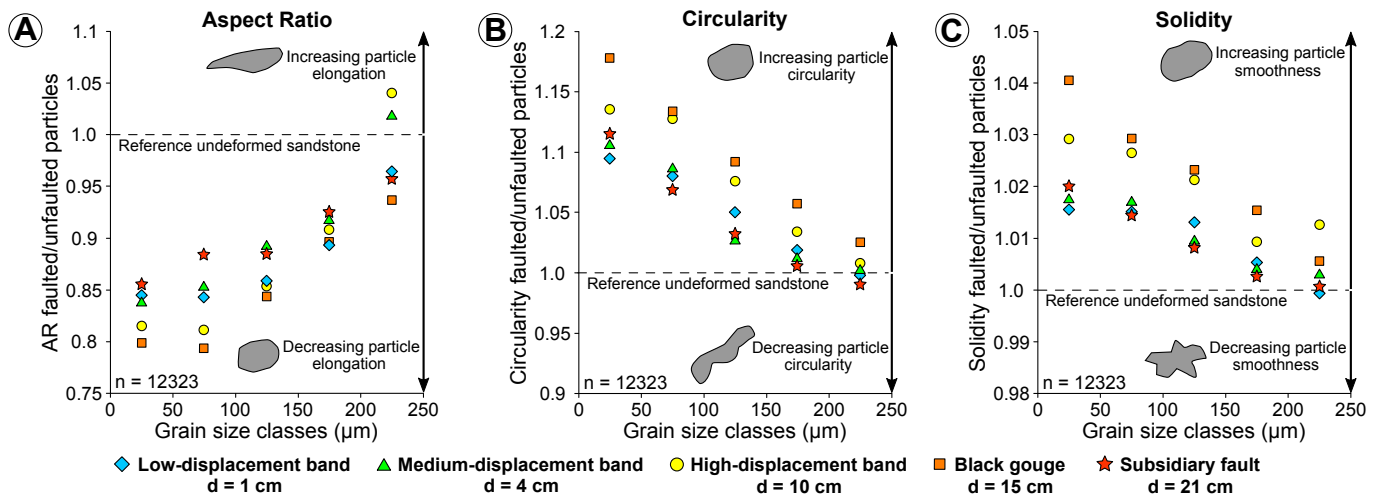


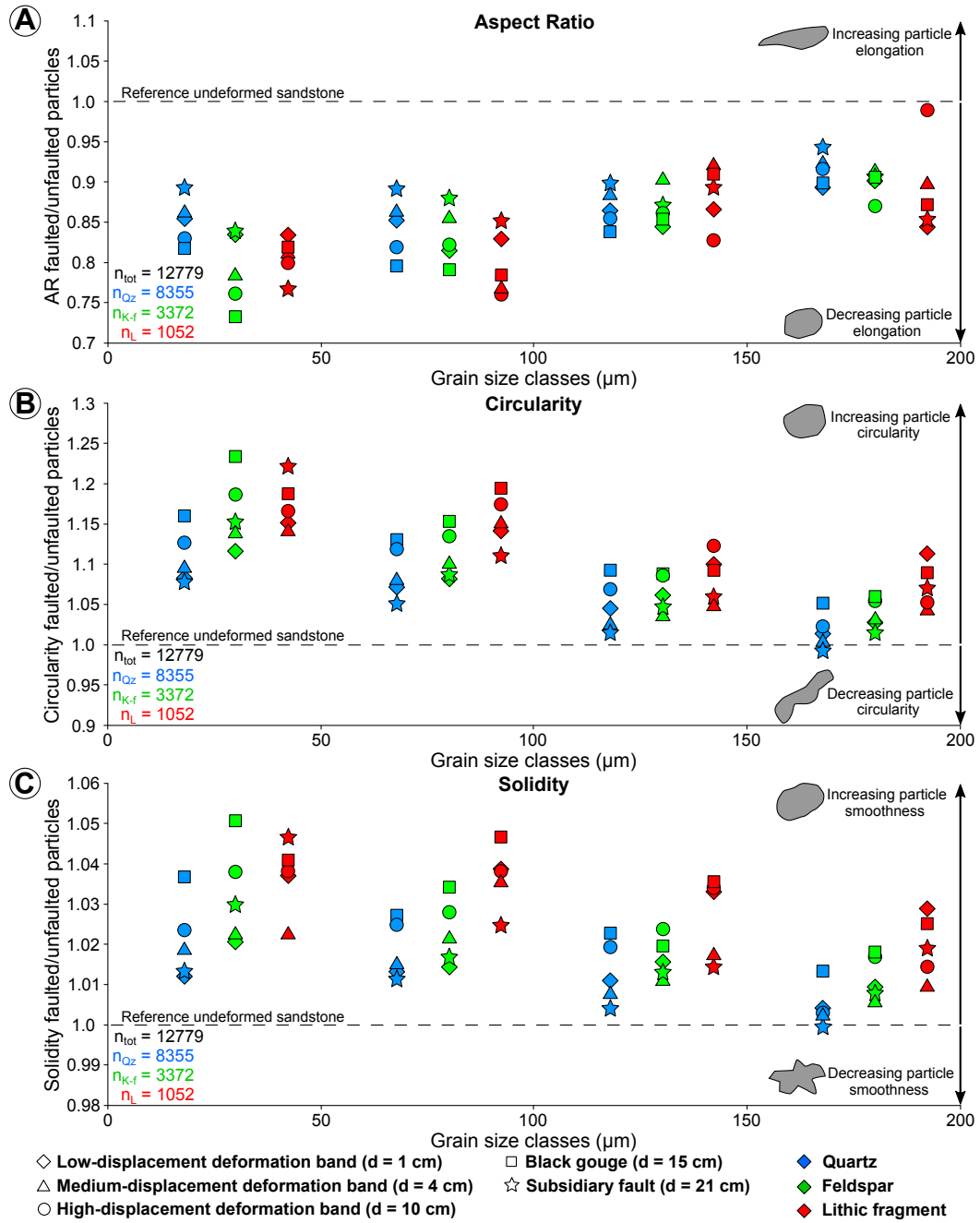


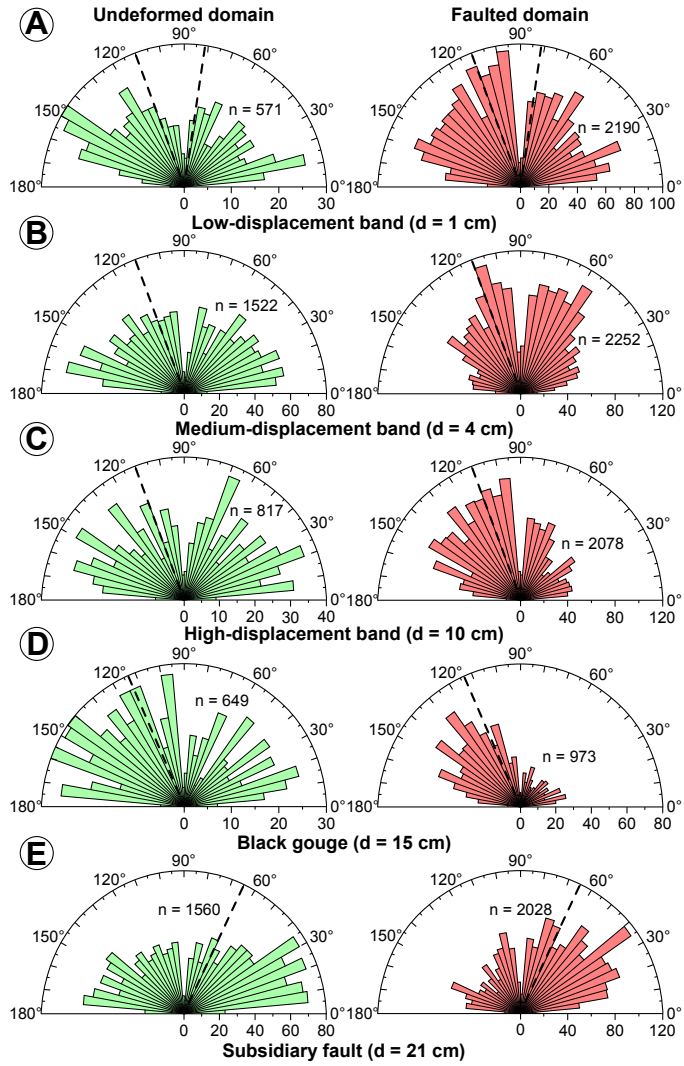


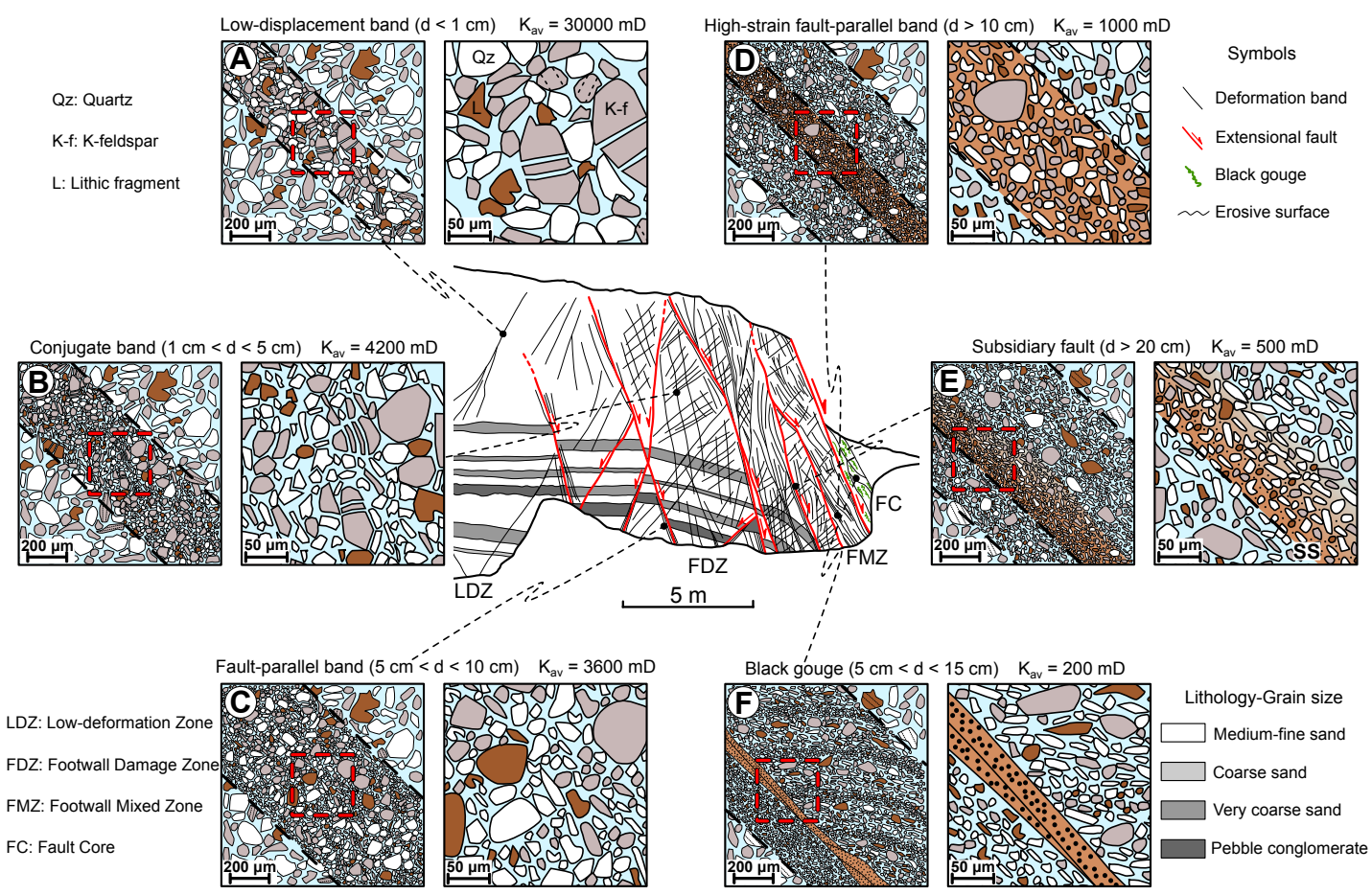


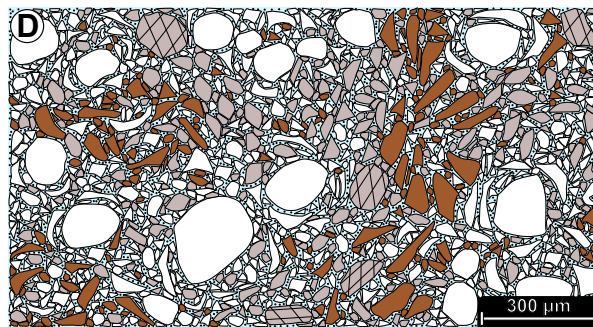
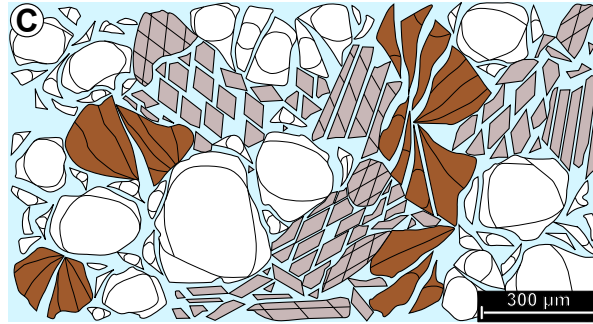
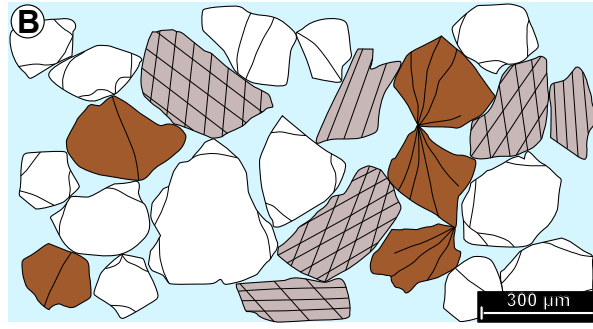
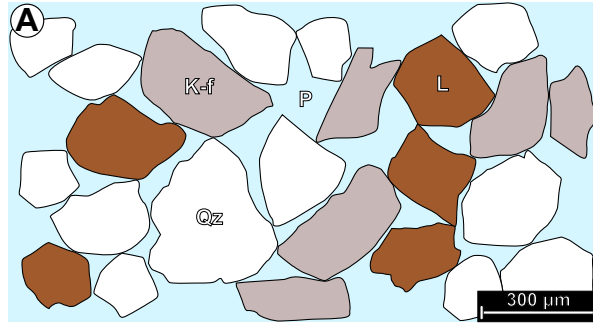






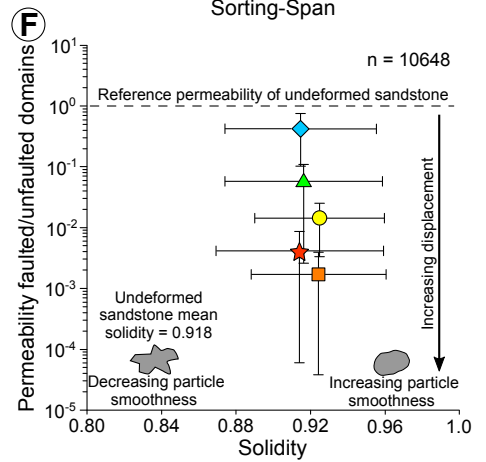
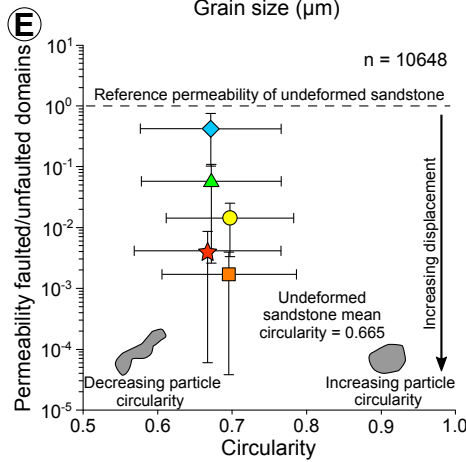
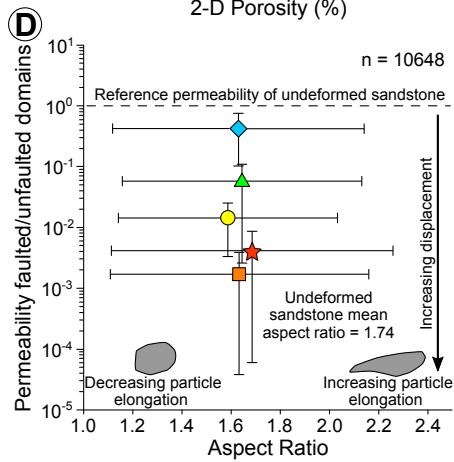
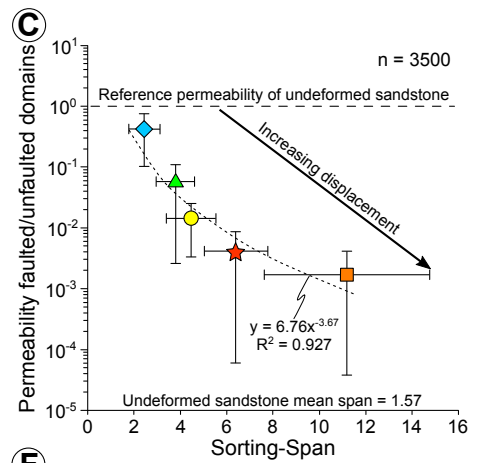
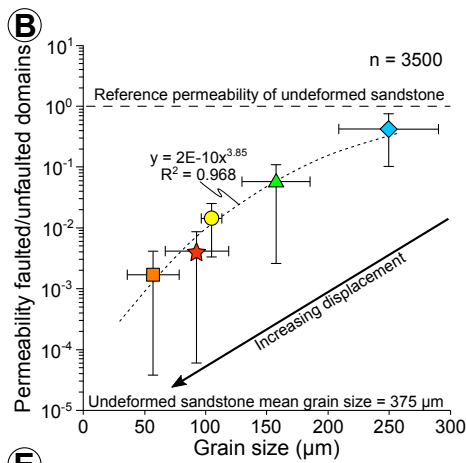
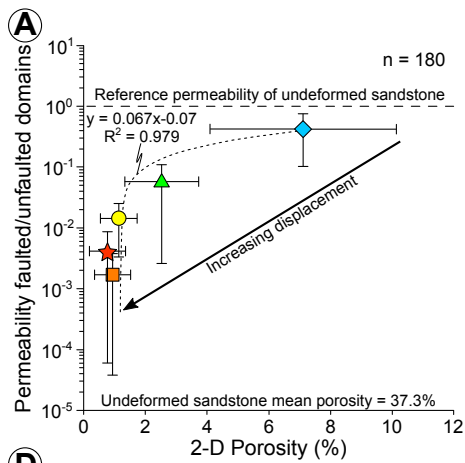




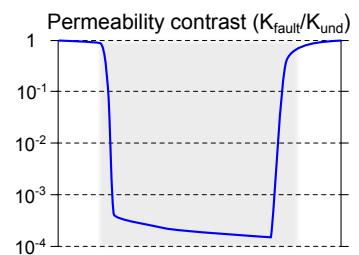
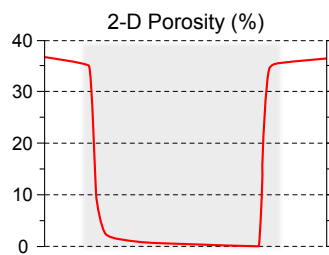
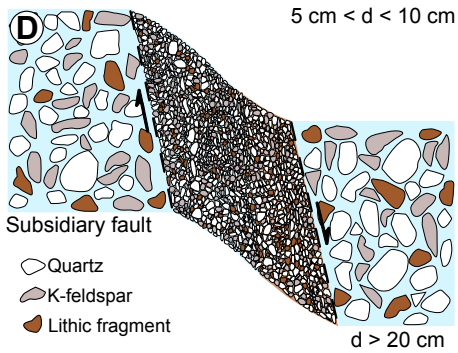
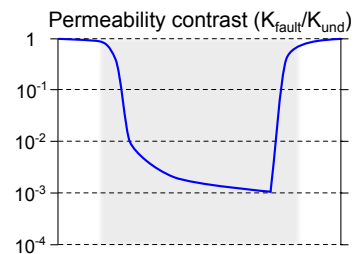
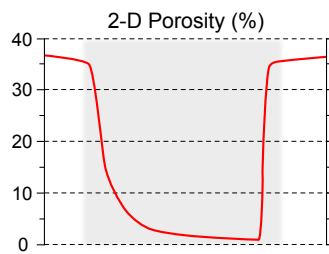
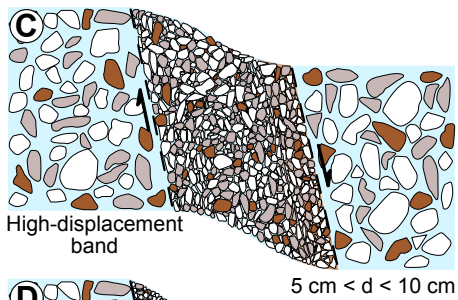
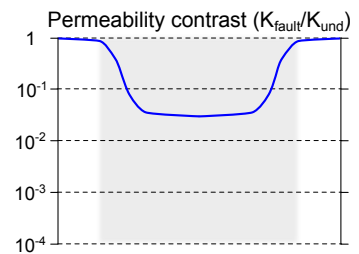
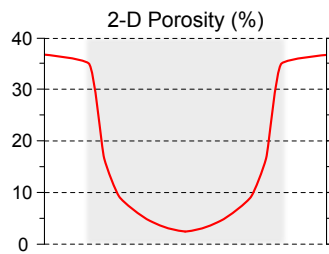
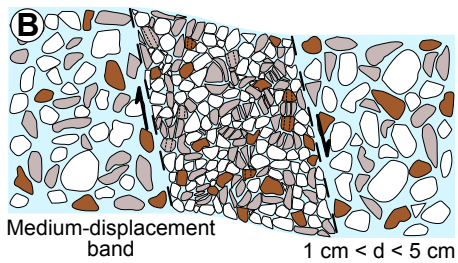
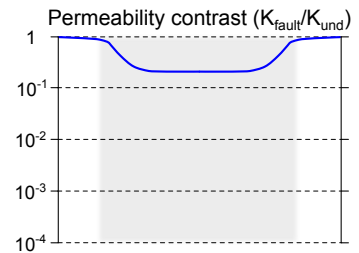
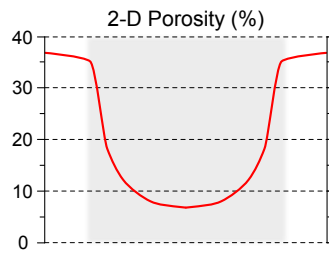
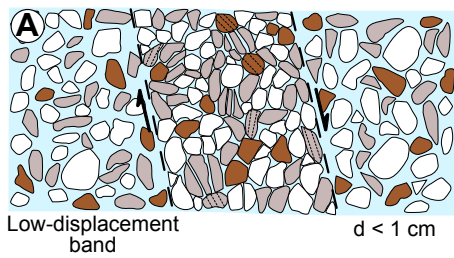


Increasing displacement and strain





◆ Low-displacement band  $d = 1$  cm    ▲ Medium-displacement band  $d = 4$  cm    ● High-displacement band  $d = 10$  cm    ■ Black gouge  $d = 15$  cm    ★ Subsidiary fault  $d = 21$  cm



Increasing displacement and strain

